FAIRCHILD SEMICONDUCTOR®

August 2008

FSDM0465RS
Green Mode Fairchild Power Switch (FPS™)

Features

- Internal Avalanche Rugged SenseFET
- Advanced Burst-Mode operation consumes under 1 W at 240V_{AC} & 0.5W load
- Precision Fixed Operating Frequency (66kHz)
- Internal Start-up Circuit
- Improved Pulse-by-Pulse Current Limiting
- Over-Voltage Protection (OVP)
- Overload Protection (OLP)
- Internal Thermal Shutdown Function (TSD)
- Abnormal Over-Current Protection (AOCP)
- Auto-Restart Mode
- Under-Voltage Lock Out (UVLO) with hysteresis
- Low Operating Current (2.5mA)
- Built-in Soft-Start

Applications

- SMPS for LCD monitor and STB
- Adaptor

Description

The FSDM0465RS is an integrated Pulse Width Modulator (PWM) and SenseFET specifically designed for high-performance offline Switch Mode Power Supplies (SMPS) with minimal external components. This device is an integrated high-voltage power-switching regulator that combines an avalanche rugged SenseFET with a current mode PWM control block. The PWM controller includes integrated fixed frequency oscillator, under-voltage lockout, leading edge blanking (LEB), optimized gate driver, internal soft-start, temperature-compensated precise-current sources for a loop compensation and self-protection circuitry. Compared with a discrete MOSFET and PWM controller solution, it can reduce total cost, component count, size and weight; while simultaneously increasing efficiency, productivity and system reliability. This device is a basic platform well suited for cost effective designs of flyback converters.

Ordering Information

Product Number	Package	Marking Code	BV_{DSS}	$R_{DS(ON)}$ Max.
FSDM0465RSWDTU(1)	TO-220F-6L(Forming)(2)	DM0465RS	650V	2.6 Ω

Note:

1. WDTU: Forming Type.
2. Pb-free package per JEDEC J-STD-020B.

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Typical Circuit

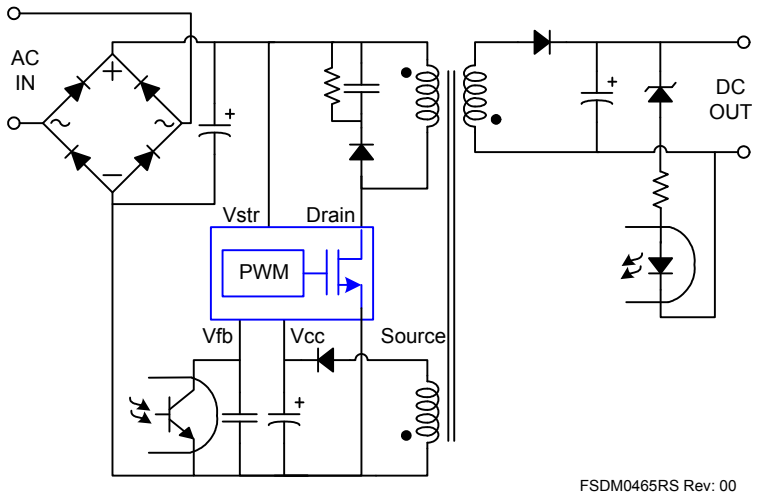


Figure 1. Typical Flyback Application

Output Power Table

Product	Maximum Output Power[3]			
	230VAC ±15%[4]		85–265VAC	
	Adapter[5]	Open Frame[6]	Adapter[5]	Open Frame[6]
FSDM0465RS	48W	56W	40W	48W

Notes:

3. The junction temperature can limit the maximum output power.
4. 230V_{AC} or 100/115V_{AC} with doubler.
5. Typical continuous power in a non-ventilated enclosed adapter measured at 50°C ambient temperature.
6. Maximum practical continuous power in an open-frame design at 50°C ambient.

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Internal Block Diagram

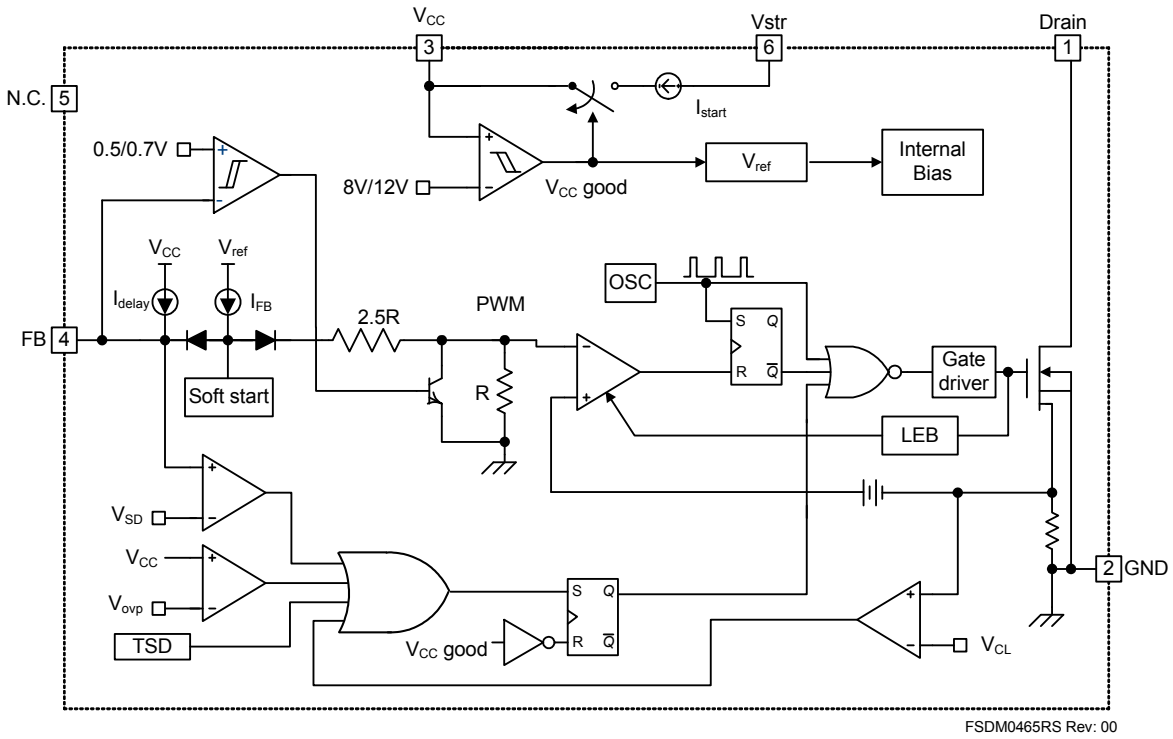


Figure 2. Functional Block Diagram of FSDM0465RS

Pin Configuration

TO-220F-6L

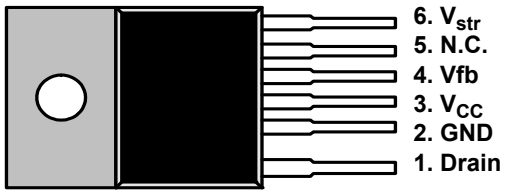


Figure 3. Pin Configuration (Top View)

Pin Definitions

Pin #	Name	Description
1	Drain	**SenseFET drain.** High-voltage power SenseFET drain connection.
2	GND	**Ground.** This pin is the control ground and the SenseFET source.
3	V_{CC}	**Power Supply.** This pin is the positive supply input, providing internal operating current for both start-up and steady-state operation.
4	Vfb	**Feedback.** This pin is internally connected to the inverting input of the PWM comparator. The collector of an opto-coupler is typically tied to this pin. For stable operation, a capacitor should be placed between this pin and GND. If the voltage of this pin reaches 6V, the overload protection triggers, which shuts down the FPS.
5	N.C.	No Connection.
6	V_{str}	**Start-up.** This pin is connected directly, or through a resistor, to the high-voltage DC link. At start-up, the internal high-voltage current source supplies internal bias and charges the external capacitor connected to the V_{CC} pin. Once V_{CC} reaches 12V, the internal current source is disabled. It is not recommended to connect V_{str} and Drain together.

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Absolute Maximum Ratings

The "Absolute Maximum Ratings" are those values beyond which the safety of the device cannot be guaranteed. The device should not be operated at these limits. The parametric values defined in the Electrical Characteristics tables are not guaranteed at the absolute maximum ratings.

T_A = 25°C, unless otherwise specified.

Symbol	Parameter		Value	Unit
BV_{DSS}	Drain Source Breakdown Voltage		650	V
V_{STR}	Vstr Max. Voltage		650	V
I_{DM}	Drain Current Pulsed(7)	Tc=25°C	9.6	A_{DC}
I_D	Continuous Drain Current(8)	Tc=25°C	2.2	A_{RMS}
		Tc=100°C	1.4	A_{RMS}
E_{AS}	Single Pulsed Avalanche Energy(9)		120	mJ
V_{CC}	Supply Voltage		20	V
V_{FB}	Input Voltage Range		-0.3 to 12	V
P_D(Watt H/S)	Total Power Dissipation (Tc=25°C)		45	W
T_j	Operating Junction Temperature		Internally limited	°C
T_A	Operating Ambient Temperature		-25 to +85	°C
T_{STG}	Storage Temperature		-55 to +150	°C
ESD	ESD Capability, HBM Model (All pins excepts for Vstr and Vfb)		2.0 (GND-Vstr/Vfb=1.5kV)	kV
	ESD Capability, Charged Device Model		1.0	kV

Notes:

7. Repetitive rating: Pulse width limited by maximum junction temperature.
8. This value is RMS current rating which should not be confused by the switching current.
9. L=14mH, starting Tj=25°C.

Thermal Impedance

T_A=25°C, unless otherwise specified.

Symbol	Parameter	Value	Unit
θ_{JA}(10)	Junction-to-Ambient Thermal	50	°C/W
θ_{JC}(11)	Junction-to-Case Thermal	2.78	°C/W

Notes:

10. Free standing with no heat-sink under natural convection.
11. Infinite cooling condition - Refer to the SEMI G30-88.

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Electrical Characteristics

T_A = 25°C unless otherwise specified.

Symbol	Parameter	Condition	Min.	Typ.	Max.	Unit
SenseFET SECTION						
I_{DSS}	Zero Gate Voltage Drain Current	V_{DS} = 650V, V_{GS} = 0V			250	μA
		V_{DS} = 520V, V_{GS} = 0V, T_C = 125°C			250	μA
$R_{DS(ON)}$	Static Drain Source on Resistance[12]	V_{GS} = 10V, I_D = 2.5A		2.2	2.6	Ω
C_{OSS}	Output Capacitance	V_{GS} = 0V, V_{DS} = 25V, f = 1MHz		60		pF
$t_{d(on)}$	Turn-on Delay Time	V_{DD} = 325V, I_D = 5A		23		ns
t_r	Rise Time			20		
$t_{d(off)}$	Turn-off Delay Time			65		
t_f	Fall Time			27		
CONTROL SECTION						
f_{OSC}	Switching Frequency	V_{FB} = 3V	60	66	72	kHz
Δf_{STABLE}	Switching Frequency Stability	13V ≤ V_{CC} ≤ 18V	0	1	3	%
Δf_{OSC}	Switching Frequency Variation[13]	-25°C ≤ T_A ≤ 85°C	0	±5	±10	%
I_{FB}	Feedback Source Current	V_{FB} = GND	0.7	0.9	1.1	mA
D_{MAX}	Maximum Duty Cycle		77	82	87	%
D_{MIN}	Minimum Duty Cycle				0	%
V_{START}	UVLO Threshold Voltage	V_{FB} = GND	11	12	13	V
V_{STOP}		V_{FB} = GND	7	8	9	V
$t_{S/S}$	Internal Soft-start Time	Vfb = 3V		10	15	ms
BURST MODE SECTION						
V_{BURH}	Burst Mode Voltages	V_{CC} = 14V		0.7		V
V_{BURL}		V_{CC} = 14V		0.5		V
PROTECTION SECTION						
V_{SD}	Shutdown Feedback Voltage	V_{FB} ≥ 5.5V	5.5	6.0	6.5	V
I_{DELAY}	Shutdown Delay Current	V_{FB} = 5V	2.8	3.5	4.2	μA
t_{LEB}	Leading Edge Blanking Time[13]			250		ns
I_{LIMIT}	Peak Current Limit[14]	V_{FB} = 5V, V_{CC} = 14V	1.6	1.8	2.0	A
V_{OVP}	Over-Voltage Protection		18	19	20	V
T_{SD}	Thermal Shutdown Temperature[13]		130	145	160	°C
TOTAL DEVICE SECTION						
I_{START}	Operating Supply Current[15]	V_{FB} = GND, V_{CC} = 11V		1	1.3	mA
I_{OP}	Operating Supply Current[15]	V_{FB} = GND, V_{CC} = 14V		2.5	5	mA
$I_{OP(MIN)}$		V_{FB} = GND, V_{CC} = 10V				
$I_{OP(MAX)}$		V_{FB} = GND, V_{CC} = 18V				

Notes:

12. Pulse test: Pulse width ≤ 300μS, duty ≤ 2%
13. These parameters, although guaranteed at the design, are not tested in mass production.
14. These parameters indicate the inductor current.
15. This parameter is the current flowing into the control IC.

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Comparison Between FS6M07652RTC and FSDM0465RS

Function	FS6M07652RTC	FSDM0465RS	FSDM0465RS Advantages
Soft-Start	Adjustable soft-start time using an external capacitor	Internal soft-start with typically 10ms (fixed)	■ Gradually increasing current limit during soft-start further reduces peak current and voltage component stresses ■ Eliminates external components used for soft-start in most applications ■ Reduces or eliminates output overshoot
Burst Mode Operation	■ Built into controller ■ Output voltage drops to around half	■ Built into controller ■ Output voltage fixed	■ Improve light load efficiency ■ Reduces no-load consumption

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Typical Performance Characteristics

(These Characteristic Graphs are Normalized at T_A= 25°C.)

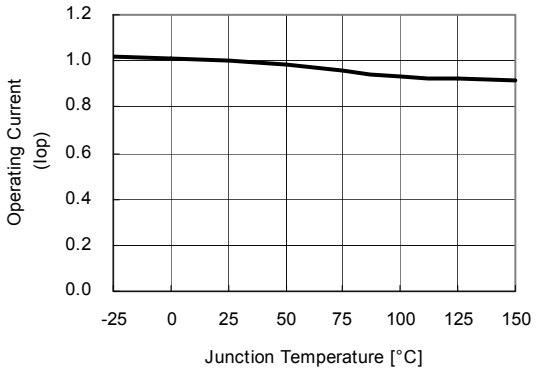


Figure 4. Operating Current vs. Temp.

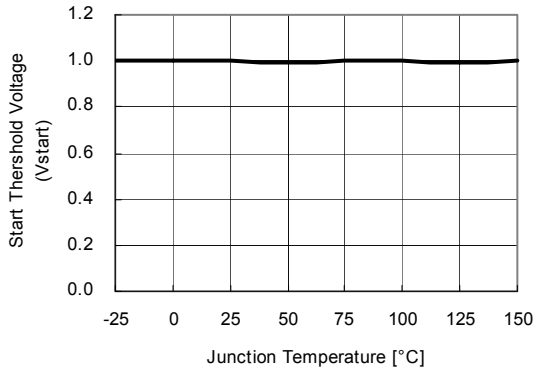


Figure 5. Start Threshold Voltage vs. Temp.

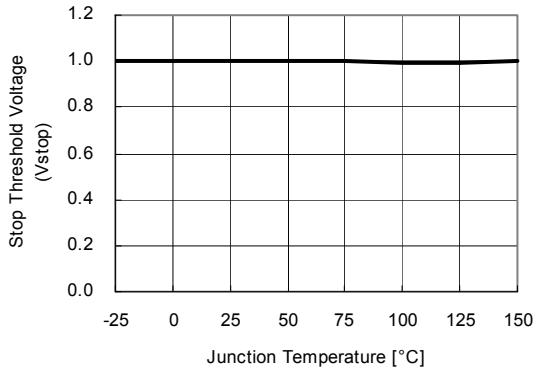


Figure 6. Stop Threshold Voltage vs. Temp.

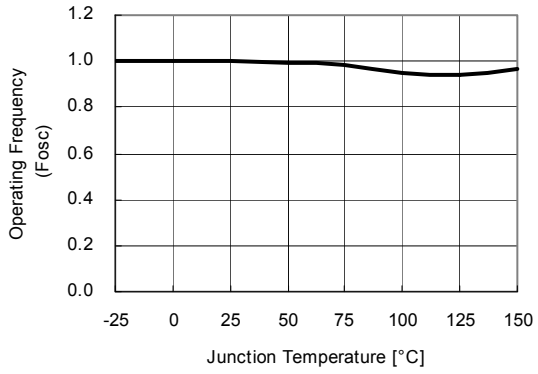


Figure 7. Operating Frequency vs. Temp.

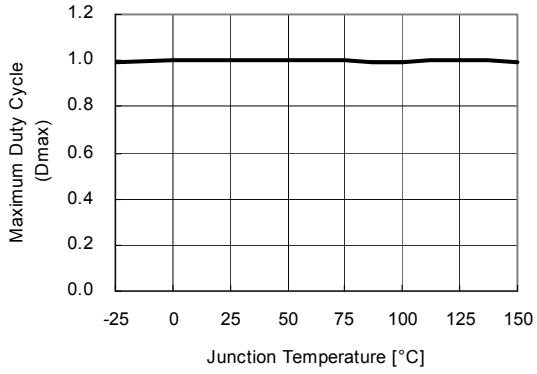


Figure 8. Maximum Duty vs. Temp.

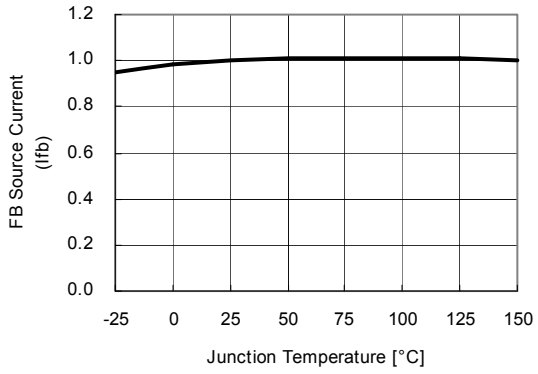


Figure 9. Feedback Source Current vs. Temp.

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Typical Performance Characteristics (Continued)

(These Characteristic Graphs are Normalized at T_A= 25°C.)

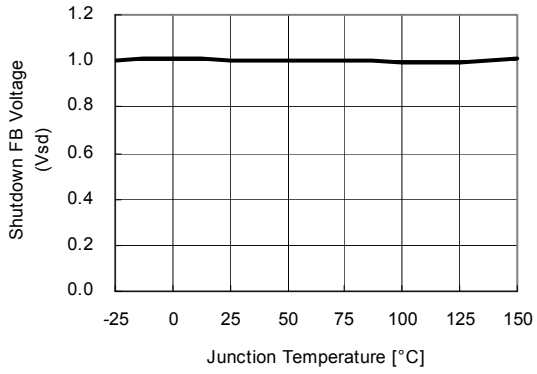


Figure 10. Shutdown Feedback Voltage vs. Temp.

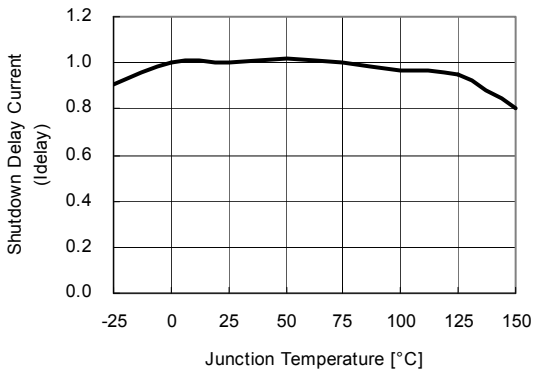


Figure 11. Shutdown Delay Current vs. Temp.

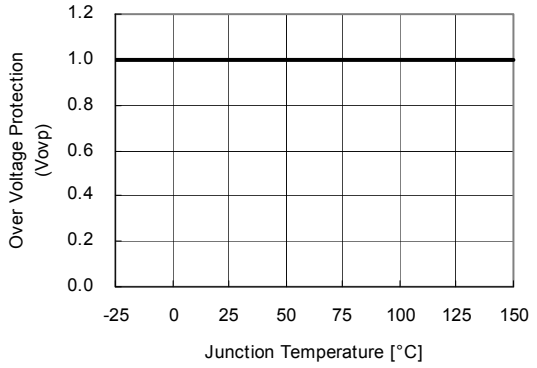


Figure 12. Over-Voltage Protection vs. Temp.

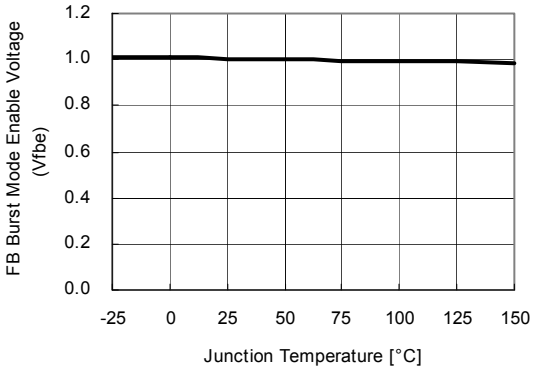


Figure 13. Burst Mode Enable Voltage vs. Temp.

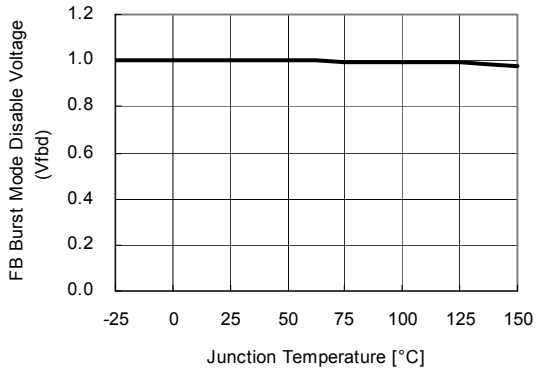


Figure 14. Burst Mode Disable Voltage vs. Temp.

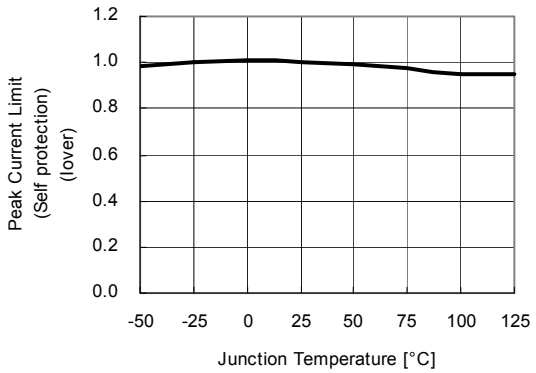


Figure 15. Current Limit vs. Temp.

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Typical Performance Characteristics (Continued)

(These Characteristic Graphs are Normalized at T_A= 25°C.)

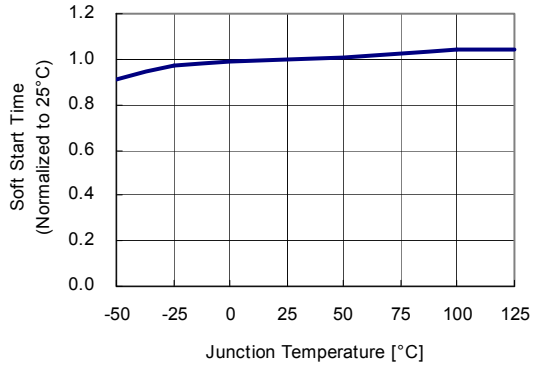


Figure 16. Soft-Start Time vs. Temp.

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Functional Description

1. Startup: In previous generations of Fairchild Power Switches (FPS™) the V_{CC} pin had an external start-up resistor to the DC input voltage line. In this generation the startup resistor is replaced by an internal high-voltage current source. At startup, an internal high-voltage current source supplies the internal bias and charges the external capacitor (C_{vcc}) that is connected to the V_{CC} pin as illustrated in Figure 17. When V_{CC} reaches 12V, the FSDM0465RS begins switching and the internal high-voltage current source is disabled. Then, the FSDM0465RS continues its normal switching operation and the power is supplied from the auxiliary transformer winding unless V_{CC} goes below the stop voltage of 8V.

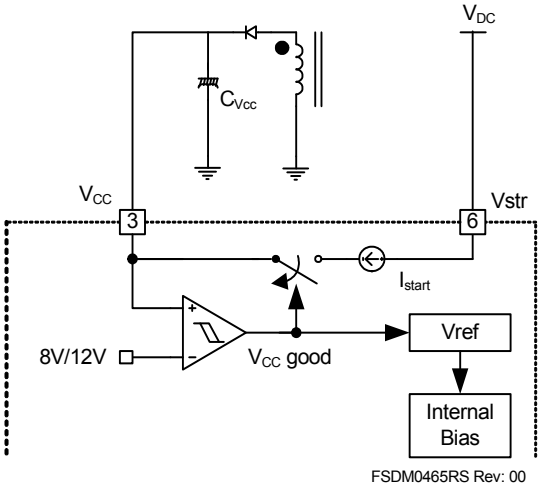


Figure 17. Internal startup circuit

2. Feedback Control: FSDM0465RS employs current mode control, as shown in Figure 18. An opto-coupler (such as the H11A817A) and shunt regulator (such as the KA431) are typically used to implement the feedback network. Comparing the feedback voltage with the voltage across the Rsense resistor plus an offset voltage makes it possible to control the switching duty cycle. When the reference pin voltage of the KA431 exceeds the internal reference voltage of 2.5V, the H11A817A LED current increases, thus pulling down the feedback voltage and reducing the duty cycle. This event typically happens when the input voltage is increased or the output load is decreased.

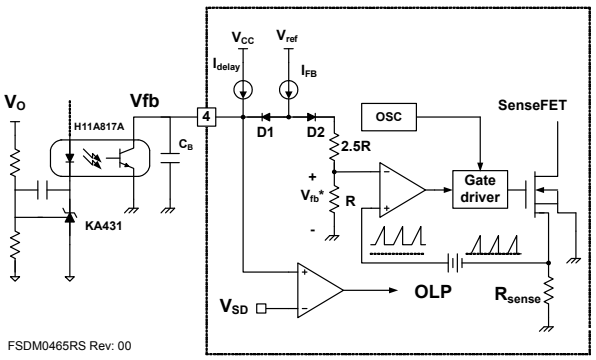


Figure 18. Pulse width modulation (PWM) circuit

2.1 Pulse-by-Pulse Current Limit: Because current mode control is employed, the peak current through the SenseFET is limited by the inverting input of PWM comparator (Vfb*) as shown in Figure 18. Assuming that the 0.9mA current source flows only through the internal resistor (2.5R + R = 2.8kΩ), the cathode voltage of diode D2 is about 2.5V. Since D1 is blocked when the feedback voltage (Vfb) exceeds 2.5V, the maximum voltage of the cathode of D2 is clamped at this voltage, thus clamping Vfb*. Therefore, the peak value of the current through the SenseFET is limited.

2.2 Leading Edge Blanking (LEB): At the instant the internal SenseFET is turned on, there usually exists a high-current spike through the SenseFET, caused by primary-side capacitance and secondary-side rectifier reverse recovery. Excessive voltage across the Rsense resistor would lead to incorrect feedback operation in the current mode PWM control. To counter this effect, the FSDM0465RS employs a leading edge blanking (LEB) circuit. This circuit inhibits the PWM comparator for a short time (t_{LEB}) after the SenseFET is turned on.

3. Protection Circuit: The FSDM0465RS has several self protective functions such as overload protection (OLP), over-voltage protection (OVP) and thermal shutdown (TSD). Because these protection circuits are fully integrated into the IC without external components, the reliability can be improved without increasing cost. Once the fault condition occurs, switching is terminated and the SenseFET remains off. This causes V_{CC} to fall. When V_{CC} reaches the UVLO stop voltage, 8V, the protection is reset and the internal high-voltage current source charges the V_{CC} capacitor via the Vstr pin. When V_{CC} reaches the UVLO start voltage, 12V, the FSDM0465RS resumes its normal operation. In this manner, the auto-restart can alternately enable and

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disable the switching of the power SenseFET until the fault condition is eliminated (see Figure 19).

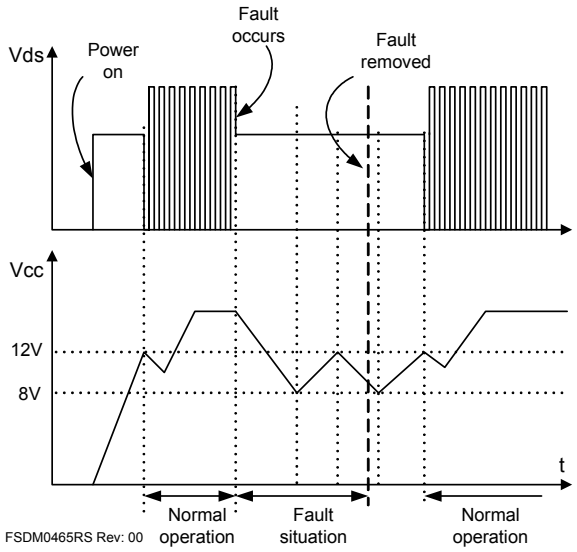


Figure 19. Auto restart operation

3.1 Overload Protection (OLP): Overload is defined as the load current exceeding a pre-set level due to an unexpected event. In this situation, the protection circuit should be activated to protect the SMPS. However, even when the SMPS is in the normal operation, the overload protection circuit can be activated during the load transition. To avoid this undesired operation, the overload protection circuit is designed to be activated after a specified time to determine whether it is a transient situation or an overload situation. Because of the pulse-by-pulse current limit capability, the maximum peak current through the SenseFET is limited, and therefore the maximum input power is restricted with a given input voltage. If the output consumes beyond this maximum power, the output voltage (V_O) decreases below the set voltage. This reduces the current through the opto-coupler LED, which also reduces the opto-coupler transistor current, thus increasing the feedback voltage (Vfb). If Vfb exceeds 2.5V, D1 is blocked and the 3.5μA current source starts to charge C_B slowly up to V_{CC}. In this condition, Vfb continues increasing until it reaches 6V, when the switching operation is terminated as shown in Figure 20. The delay time for shutdown is the time required to charge C_B from 2.5V to 6.0V with 3.5μA. In general, a 10 ~ 50 ms delay time is typical for most applications.

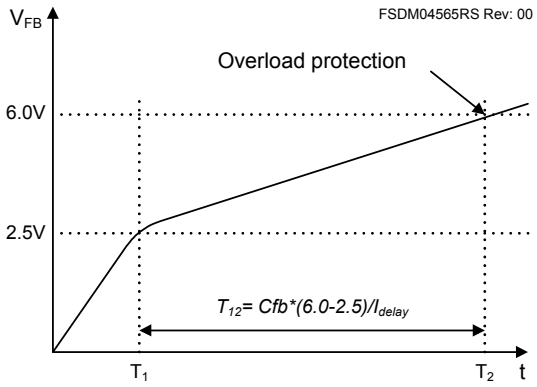


Figure 20. Overload protection

3.2 Over-voltage Protection (OVP): If the secondary side feedback circuit were to malfunction or a solder defect caused an open in the feedback path, the current through the opto-coupler transistor becomes almost zero. Then, Vfb climbs up in a similar manner to the overload situation, forcing the preset maximum current to be supplied to the SMPS until the overload protection is activated. Because more energy than required is provided to the output, the output voltage may exceed the rated voltage before the overload protection is activated, resulting in the breakdown of the devices in the secondary side. To prevent this situation, an over-voltage protection (OVP) circuit is employed. In general, V_{CC} is proportional to the output voltage and the FSDM0465RS uses V_{CC} instead of directly monitoring the output voltage. If V_{CC} exceeds 19V, an OVP circuit is activated resulting in the termination of the switching operation. To avoid undesired activation of OVP during normal operation, V_{CC} should be designed to be below 19V.

3.3 Thermal Shutdown (TSD): The SenseFET and the control IC are built in one package. This makes it easy for the control IC to detect the heat generation from the SenseFET. When the temperature exceeds approximately 150°C, the thermal shutdown is activated.

4.2 Abnormal Over-Current Protection (AOCP): When the secondary rectifier diodes or the transformer pins are shorted, a steep current with extremely high di/dt can flow through the SenseFET during the LEB time. Even though the FPS has overload protection, it is not enough to protect the FPS in those abnormal cases, since severe current stress is imposed on the SenseFET until OLP triggers. This IC has an internal AOCP circuit shown in Figure 21. When the gate turn-on signal is applied to the power SenseFET, the AOCP block is enabled and monitors the current through the sensing resistor. The voltage across the resistor is compared with a preset AOCP level. If the sensing resistor voltage is

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greater than the AOCP level, the set signal is applied to the latch, resulting in the shutdown of the SMPS.

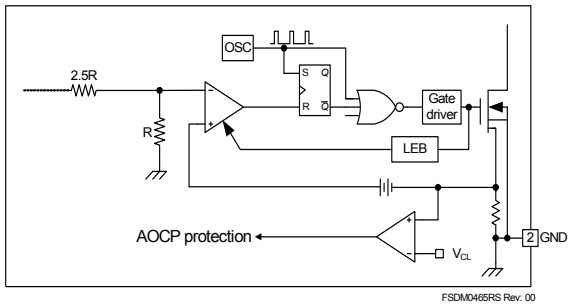


Figure 21. Abnormal Over-Current Protection

4. Soft-Start: The FSDM0465RS has an internal soft-start circuit that increases PWM comparator inverting input voltage together with the SenseFET current slowly after it starts up. The typical soft-start time is 10msec, The pulse width to the power switching device is progressively increased to establish the correct working conditions for transformers, inductors, and capacitors. The voltage on the output capacitors is progressively increased with the intention of smoothly establishing the required output voltage. It also helps to prevent transformer saturation and reduce the stress on the secondary diode during startup.

5. Burst operation: To minimize power dissipation in standby mode, the FSDM0465RS enters burst mode operation. As the load decreases, the feedback voltage decreases. As shown in Figure 22, the device automatically enters burst mode when the feedback voltage drops below V_{BURL}(500mV). At this point switching stops and the output voltages start to drop at a rate dependent on standby current load. This causes the feedback voltage to rise. Once it passes V_{BURH}(700mV) switching resumes. The feedback voltage then falls and the process repeats. Burst mode operation alternately enables and disables switching of the power SenseFET thereby reducing switching loss in Standby mode.

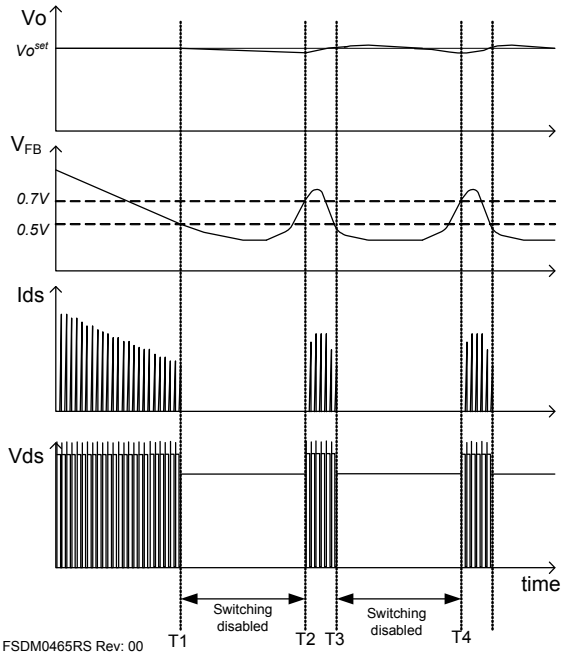


Figure 22. Waveforms of Burst Operation

Typical application circuit

Application	Output power	Input voltage	Output voltage (Max current)
LCD Monitor	34W	Universal input (85-265Vac)	5V (2.0A) 12V (2.0A)

Features

- High efficiency (>81% at 85Vac input)
- Low zero load power consumption (<300mW at 240Vac input)
- Low standby mode power consumption (<800mW at 240Vac input and 0.3W load)
- Low component count
- Enhanced system reliability through various protection functions
- Internal soft-start (10ms)

Key Design Notes

- Resistors R102 and R105 are employed to prevent start-up at low input voltage. After startup, there is no power loss in these resistors since the startup pin is internally disconnected after start-up.
- The delay time for overload protection is designed to be about 50ms with C106 of 47nF. If a faster triggering of OLP is required, C106 can be reduced to 10nF.
- Zener diode ZD102 is used for a safety test such as UL. When the drain pin and feedback pin are shorted, the zener diode fails and remains short, which causes the fuse (F1) blown and prevents explosion of the opto-coupler (IC301). This zener diode also increases the immunity against line surge.

1. Schematic

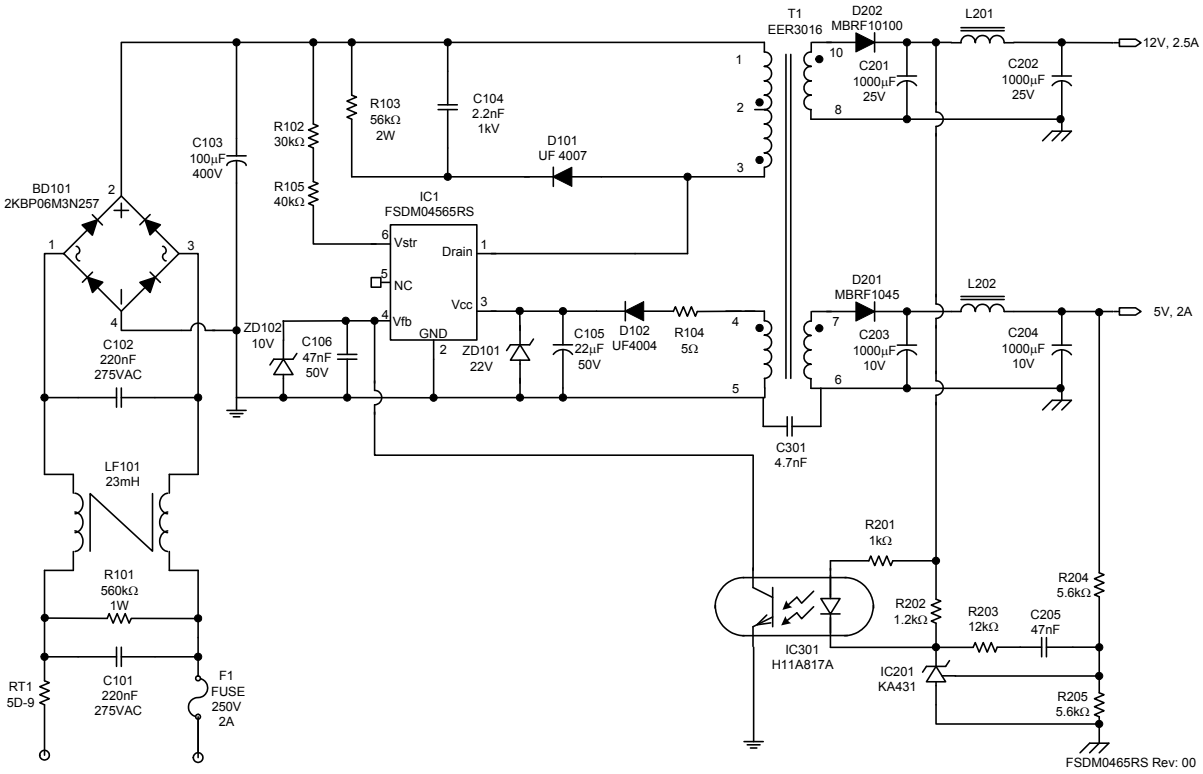


Figure 23. Demo Circuit

2. Transformer

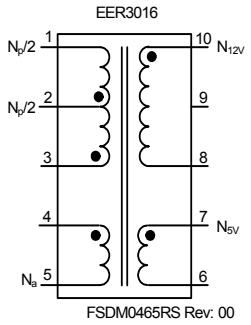


Figure 24. Transformer Schematic Diagram

3.Winding Specification

No	Pin (s→f)	Wire	Turns	Winding Method
Na	4 → 5	$0.2^{\phi} \times 1$	8	Center Winding
Insulation: Polyester Tape t = 0.050mm, 2 Layers				
Np/2	2 → 1	$0.4^{\phi} \times 1$	18	Solenoid Winding
Insulation: Polyester Tape t = 0.050mm, 2 Layers				
N_{12V}	10 → 8	$0.3^{\phi} \times 3$	7	Center Winding
Insulation: Polyester Tape t = 0.050mm, 2 Layers				
N5V	7 → 6	$0.3^{\phi} \times 3$	3	Center Winding
Insulation: Polyester Tape t = 0.050mm, 2 Layers				
Np/2	3 → 2	$0.4^{\phi} \times 1$	18	Solenoid Winding
Outer Insulation: Polyester Tape t = 0.050mm, 2 Layers				

4.Electrical Characteristics

	Pin	Specification	Remarks
Inductance	1 - 3	650μH ± 10%	100kHz, 1V
Leakage Inductance	1 - 3	10μH Max	2^{nd} all short

5. Core & Bobbin

- Core: EER 3016
- Bobbin: EER3016
- Ae(mm2): 96

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6. Demo Circuit Part List

Part	Value	Note	Part	Value	Note
Fuse			**Inductor**		
F101	2A/250V		L201	5μH	Wire 1.2mm
NTC			L202	5μH	Wire 1.2mm
RT101	5D-9		**Diode**		
Resistor			D101	UF4007	
R101	560kΩ	1W	D102	UF4004	
R102	30kΩ	1/4W	D201	MBRF1045	
R103	56kΩ	2W	D202	MBRF10100	
R104	5Ω	1/4W	ZD101	Zener Diode	22V
R105	40kΩ	1/4W	ZD102	Zener Diode	10V
R201	1kΩ	1/4W	**Bridge Diode**		
R202	1.2kΩ	1/4W	BD101	2KBP06M 3N257	Bridge Diode
R203	12kΩ	1/4W			
R204	5.6kΩ	1/4W	**Line Filter**		
R205	5.6kΩ	1/4W	LF101	23mH	Wire 0.4mm
			IC		
Capacitor			IC101	FSDM0465RS	FPS™
C101	220nF/275VAC	Box Capacitor	IC201	KA431 (TL431)	Voltage reference
C102	220nF/275VAC	Box Capacitor	IC301	H11A817A	Opto-coupler
C103	100μF/400V	Electrolytic Capacitor			
C104	2.2nF/1kV	Ceramic Capacitor			
C105	22uF/50V	Electrolytic Capacitor			
C106	47nF/50V	Ceramic Capacitor			
C201	1000μF/25V	Electrolytic Capacitor			
C202	1000μF/25V	Electrolytic Capacitor			
C203	1000μF/10V	Electrolytic Capacitor			
C204	1000μF/10V	Electrolytic Capacitor			
C205	47nF/50V	Ceramic Capacitor			
C301	4.7nF	Polyester Film Cap.			

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7. Layout

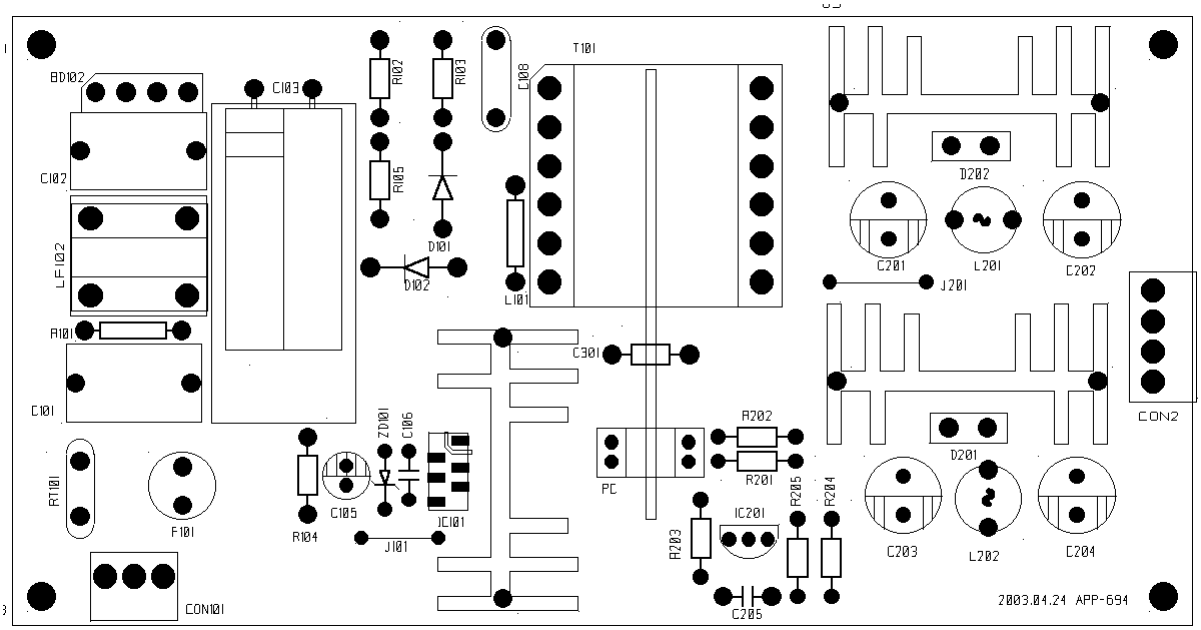


Figure 25. Layout Considerations for FSDM0465RS

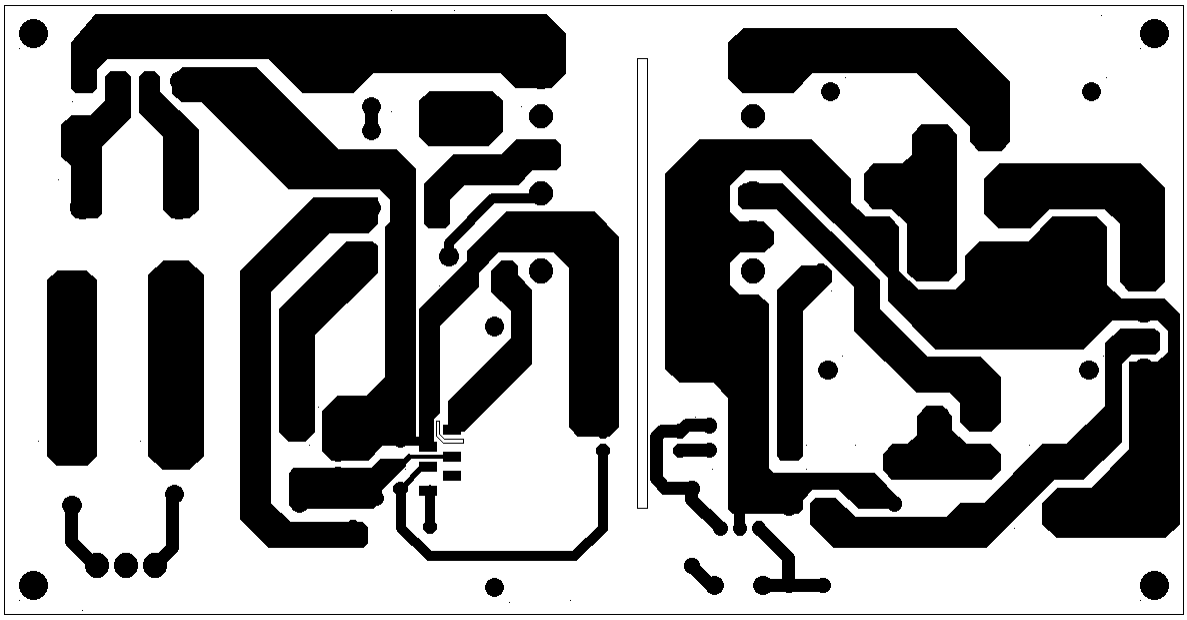
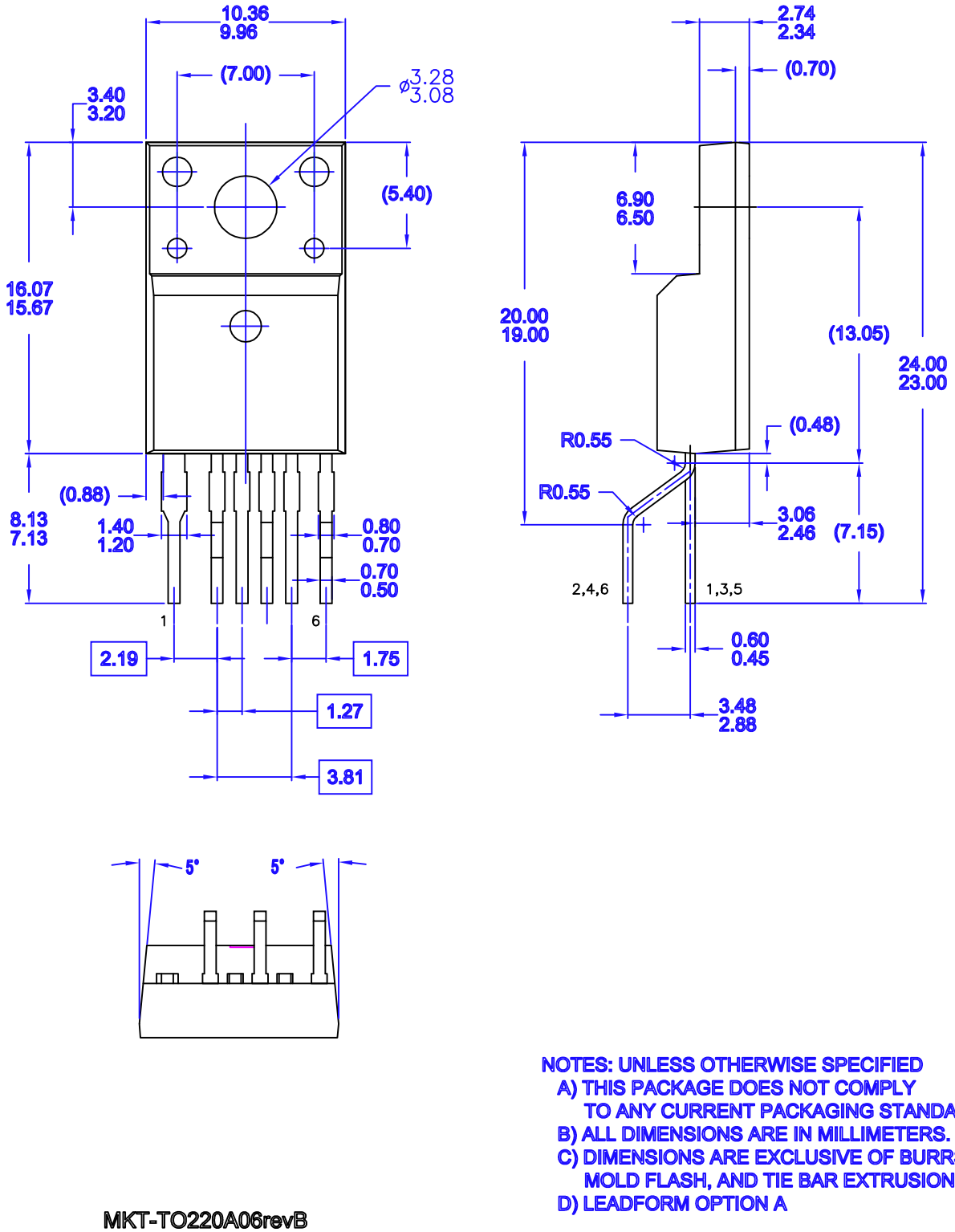


Figure 26. Layout Considerations for FSDM0465RS

Package Dimensions

TO-220F-6L (Forming)

Dimensions in millimeters



MKT-TO220A06revB

NOTES: UNLESS OTHERWISE SPECIFIED
A) THIS PACKAGE DOES NOT COMPLY TO ANY CURRENT PACKAGING STANDARD.
B) ALL DIMENSIONS ARE IN MILLIMETERS.
C) DIMENSIONS ARE EXCLUSIVE OF BURRS, MOLD FLASH, AND TIE BAR EXTRUSIONS.
D) LEADFORM OPTION A

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EnSigna™	MICROCOUPLER™	QFET®	SyncFET™	VCX™
FACT™	MicroFET™	QS™	TCM™	Wire™
FACT Quiet Series™	MicroPak™	QT Optoelectronics™	TinyBoost™	
FAST®	MICROWIRE™	Quiet Series™		
FASTr™	MSX™	RapidConfigure™	Across the board. Around the world.™	
FPS™	MSXPro™	RapidConnect™	Programmable Active Droop™	
FRFET™	OCX™	ScalarPump™	The Power Franchise®	

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