Power Factor Corrected LED Boost Switching Regulator

The NCL30167 high power factor boost PWM switching regulator is designed to regulate the average current through a string of LEDs. The circuit operates in Critical Conduction Mode (CrM) based on a proven constant on-time control scheme to achieve near unity power factor. In addition to regulating a constant current, the switching regulator is optimized to support leading and trailing edge phase dimming applications. When a dimmer is detected on the AC input, an internal voltage reference of the current regulation loop adjusts the current level based on the dimmer conduction angle so the current through the LED string has a desired value based on a programmed dimming curve. The shape of the dimming curve is intended to emulate the response of an incandescent bulb while achieving NEMA SSL6 and NEMA SSL7A recommendations.

A cascoded configuration supports biasing the controller during operation and eliminates the need for an auxiliary winding to provide bias power. A robust suite of protection features are included to ensure proper handling of expected fault conditions without the need for extra circuitry and a dedicated thermal fold-back input proves gradually reduction of the current above a user defined set-point.

Features

- Near-Unity Power Factor
- Critical Conduction Mode (CrM)
- Constant On-time Control
- Accurate Current Regulation (±2% Typical)
- Compatible with Leading and Trailing Edge Phase Controlled Dimmers
- Fast Startup Time $(< 100 \text{ ms}$ Typical)
- Integrated ZCD Detection
- User Programmable Thermal Current Fold-back
- V_{CC} Operation up to 20 V
- This Device is Pb-Free and is RoHS Compliant

Safety Features

- Output Overvoltage Protection
- Cycle-by-Cycle Current Limiting
- \bullet V_{CC} UVLO

Typical Applications

- LED Bulbs
- LED Downlights
- LED Light Engines
- LED Modules

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MARKING DIAGRAM 10 H H H H H II 30167 ALYWX -1 L30167 = Specific Device Code A = Assembly Location

- $L = Water Lot$
 $Y = Year$ $=$ Year
- $W = Work Week$
- -= Pb−Free Package

(Note: Microdot may be in either location)

PIN CONNECTIONS

ORDERING INFORMATION

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specification Brochure, BRD8011/D.

TYPICAL APPLICATION EXAMPLE

PIN FUNCTION DESCRIPTION

Table 1. PIN FUNCTION DESCRIPTION

SIMPLIFIED INTERNAL BLOCK SCHEMATIC

Table 2. MAXIMUM RATINGS

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

1. Limited by the junction temperature.

2. This device contains ESD protection and exceeds the following tests: Human Body Model 3500 V per JEDEC Standard JESD22−A114E, Machine Model Method 250 V per JEDEC Standard JESD22−A115B, Charged Device Model 1000 V per JEDEC Standard JESD22−C101E.

3. This device contains Latch-up protection and has been tested per JEDEC JESD78D, Class I and exceeds ±100 mA.

Table 3. ELECTRICAL CHARACTERISTICS

(For typical values T_j = 25°C, for min/max values T_j = –40°C to +125°C, V_{CC} = 13 V unless otherwise noted)

Table [3.](#page-4-0) ELECTRICAL CHARACTERISTICS (continued)

(For typical values T_j = 25°C, for min/max values T_j = –40°C to +125°C, V_{CC} = 13 V unless otherwise noted)

Table [3.](#page-4-0) ELECTRICAL CHARACTERISTICS (continued)

(For typical values T_j = 25°C, for min/max values T_j = –40°C to +125°C, V_{CC} = 13 V unless otherwise noted)

Product parametric performance is indicated in the Electrical Characteristics for the listed test conditions, unless otherwise noted. Product performance may not be indicated by the Electrical Characteristics if operated under different conditions.

1. Guaranteed by design.

Figure 5. V_{CC} Decreasing Level at which the **Internal Logic Resets, V_{CC(reset)}**

Figure 3. Turn-On Threshold Level, V_{CC(on)} Figure 4. Minimum Operating Voltage, V_{CC(off)}

Figure 6. Internal Current Consumption before Start-Up, I_{CC1}

Figure 8. Internal Current Consumption when DRV Pin is Turned-On, I_{CC3}

Figure 10. Over-Voltage Protection Threshold (V_{OVP} Going Down), V_{OVP(on)}

Figure 12. Under-Voltage Detect Threshold, V_{UVP}

Figure 14. Minimum Internal Current Set-Point, VILIM_MIN

Figure 17. Lower ZCD Threshold, V_{ZCD(falling)} Figure 18. Upper ZCD Threshold, V_{ZCD(rising)}

Figure 19. Current Sense Threshold for CS2 Pin Open Protection, V_{CS2(stop)}

Figure 16. Internal Reference for Nominal LED Current, VREF

Figure 20. Dimming Detection Comparator Threshold, V_{ACCTН} Going Up, V_{ACCTН} н

Figure 22. TF Pin Voltage at which Thermal Fold-Back Starts, VTF(start)

Figure 24. Current Source for Direct NTC Connection, I_{TF}

Figure 26. Typical On-Time of the Internal Driving Switch

Figure 27. Typical Off-Time of the Internal Driving Switch

APPLICATION INFORMATION

Functional Description

NCL30167 uses a Constant On-time Boost architecture in order to target a unity power factor, when no dimming is detected. The cascoded drain architecture shown in Figure 28, where $M_{\text{HV ext}}$ is the High Voltage Cascode NMOS, allows a simple implementation of a V_{CC} supply by including a diode D_{VCC} , external to the switcher IC, between the DRAIN pin and capacitor C_{VCC} . Thanks to the cascoded drain architecture, the startup time is very fast (typ < 100 ms). Unlike a traditional asynchronous boost architecture, the cascoded architecture uses two MOSFETS. The low voltage MOSFET M_{LV} int., which is housed inside the IC, drives the external High Voltage NMOS M_{HV} ext via the DRV pin.

Figure 28. Cascode Architecture

The NCL30167 operates in Critical Conduction Mode (CrM) under all working conditions, regulating the average current flowing through the string of LEDs whether the dimmer is present or not.

The ACC_TH pin senses a scaled down input voltage (Vin) and by comparing it to an internal reference voltage named VACC_TH it provides a digital signal DIM/DIMb that contains the amount of dimming information. DIM/DIMb is processed then by a circuit block named "Vref processing", which provides analog signal Vref. The reference voltage named Vref serves for the LED current regulation loop. The LED current regulation loop is working for all conduction angles, it is then possible by programming the Vref processing circuit block to get the desired dimming curve as depicted in Figure [30](#page-14-0).

Critical Conduction Mode

By looking at Figure [28](#page-12-0) it can be seen that, the current I_{Rsense1} flowing through the external resistor R_{sense1}, connected between pin CS1 and GND, is the same as the inductor current I_{ind} plus current spikes associated with the turning on or turning off of M_{LV} int NMOS FET. The inductor current information carried by the pin CS1 is used for the inductor peak current limitation. This voltage V_{CS1} is used to generate a reset signal (OCP_RST) resulting from having reached the inductor maximum peak current controlled by V_{ILIM} reference voltage. If the maximum peak inductor current is not reached it is the second branch that takes care of the reset signal (RST) indicating the end of the on-time. The second branch monitors the off-time current information at current sense input CS2. The CS2 sensing is inhibited during the MOSFET on-time.

As shown in Figure [2,](#page-3-0) the second branch voltage is an image of the off-time inductor current. It is sent to the input of an OTA and by comparing to a reference voltage (V_{REF}) a control voltage is generated at the COMP pin. The COMP pin voltage is proportional to the average LED current. It is compared to a constant on-time ramp voltage generated by charging the capacitor C_{TON} by a constant current I_{TON} . The output of the comparator generates constant on-time reset signal (RST). This process represents the "constant t_{on} average LED regulation loop" which, when steady state is reached, ensures that:

$$
I_{LEDay} = \frac{V_{REF}}{R_{sense2}}
$$
 (eq. 1)

There is one more condition to end the on-time cycle. The power MOSFET is turned-off only under a condition that the inductor peak current reaches a level set by the reference voltage named V_{ILIM MIN}. Minimum input current is maintained by switching in Constant Peak Current mode. When a dimmer is present this feature helps to avoid the leakage current of the dimmer from charging the C_{in} capacitor. At the same time this feature sets a minimum input current to avoid the current loop cut off when the triac dimming is applied.

The reset signal (RST or OCP_RST) indicates an end of the on-time and a start of the off-time. Once the off-time has started, the CS2 pin senses the inductor off-time current across R_{sense2} . It is compared to a reference voltage V_{ZCD} in order to generate a zero-crossing signal (ZCD) that in turn is processed by the clock generation block. The generated clock pulse triggers a start of the new on-time cycle.

LED Current Regulation and Dimming Curve

As long as the max peak current limitation is not exceeded or a thermal foldback condition is present, the average LED current regulation loop is controlled by the OTA via Equation 1 and Triac Dimming Curve of Figure 30.

For example if $R_{\text{sense2}} = 20 \Omega$ and $V_{\text{REF}} = 0.5 V$ it gives $I_{LED} = 25$ mA. The circuit block named V_{REF} processing which can be seen in Figure [2](#page-3-0) will be programmed for the optimum compatibility acceleration curve by default (see Figure [30](#page-14-0)) with an option of the optimum diming acceleration curve.

To regulate an average LED current in a single stage architecture the instantaneous LED current can have as much as ±50% ripple component (this ripple component depends on the value of C_{out} capacitor and LED string dynamic resistance). The OTA must work linearly while a voltage with ripple is applied. The transconductance (G_m) value is set as low as $100 \mu S$ and the minimal output current capability is at ± 40 µA to ensure the OTA linear operation, without entering the saturation level.

Dimming Presence Sensing

The conduction angle of the dimmer is sensed through pin ACC_TH . The rectified and dimmed V_{in} voltage (see Figure [1](#page-1-0)) appears on pin ACC_TH divided by the resistor bridge composed of $R_{\text{acc_top}}$ and $R_{\text{acc_bot}}$. The ACC_TH voltage is equal to:

$$
V_{ACC_TH} = K_{acc} \cdot V_{in}
$$
 (eq. 2)

where:

$$
K_{\text{acc}} = \frac{R_{\text{acc_bot}}}{R_{\text{acc_bot}} + R_{\text{acc_top}}} \tag{eq. 3}
$$

Figure 31. ACC_TH Pin Waveforms and Max/Min Detectable Dimmer Conduction Angles

Voltage sensed at the ACC_TH pin is compared to the V_{ACC} TH reference voltage (see Figure [31\)](#page-15-0) in order to generate a digital signal (DIM/DIMbar) (see Figure [2](#page-3-0) and Figure 32). The DIM/DIMbar signal is used as the input of the block named "Vref processing block". Every half period of the mains voltage, the "Vref processing block" computes and holds the dimmer duty cycle and sets the corresponding VREF voltage.

Unless the minimum peak current at CS1 pin reaches the $V_{IIIM MIN}$ level the internal power MOSFET connected between DRAIN and CS pins is kept open to avoid a leakage current of the dimmer from charging the C_{in} capacitor (see Figure [1](#page-1-0)) and providing a low impedance path for "SMART" dimmer operation.

CA is the Dimmer Conduction Angle expressed in degrees and can be calculated based on the Dimmer Conduction Time t_{CA} (see Figure 32) and the AC mains frequency fmains described in the following formula:

$$
CA = 360 \cdot t_{CA} \cdot f_{\text{mains}} \tag{eq. 4}
$$

Detailed Description of the V_{REF} Processing

The conduction angle is obtained by the digital division of the sampled values of the conduction time and the period. The conduction time is counted by the timer A over the both periods of mains as the period of mains. This type of sensing decreases the diming system sensitivity to the asymmetry of the diming triac and reduces flickering. The conducting angle is obtained as the ratio of Timer A (conduction time) and Timer B (the mains period). Please refer to Figure [33](#page-17-0) and Figure [34](#page-17-0).

$$
CA = \frac{2 \cdot T_{on}}{2 \cdot T}
$$
 (eq. 5)

The additional IIR filters and the conduction angle lockout for 32 cycles of the rectified mains signal helps to reduce flickering caused by the differing leading edges and quantization error of the A/D conversion at TF pin and CA measurement.

Figure 33. Detailed Block Schematic of the Conduction Angle Measurement and the V_{REF} Processing

Figure 34. Time Diagram of the Implemented Conduction Angle Measurement

The minimum current set-point feature is implemented. It starts play a role in case when the Vref is so small that the current set-point observed at CS1 pin is below the VILIM_MIN level. Then the regulation loop requirement is ignored and higher level of current set-point V_{ILIM_MIN} is

applied. This feature sets the minimum current to avoid the current loop cut off when the triac dimming is applied. This feature increases the compatibility with the most of the triac dimmers.

Figure 35. The Minimum Current Set-Point Effect to Keep the Loop Current

CS2 ZCD Timeout Protection

The second CS2 pin has an additional feature. In case of very low average current is regulated the CS2 voltage can be too low. The CS2 sensed voltage can be too low so that the CS2 ZCD is not detected. To avoid stopping the device under this condition the ZCD timeout feature is added. If no ZCD event is detected until the ZCD timer (t_{ZCD(timeout)}) elapses the internal cascode switch is turned on anyway.

Figure 36. CS2 Pin ZCD Timeout Protection − Principal Diagram

Protection Against a Winding Short

Under some conditions, such as a winding short-circuit of the boost inductor, the on-time duration is at a minimum (based on the internal propagation delay of the detector and LEB duration). In this event, the current sense voltage increases above V_{ILIM} , because the controller is blanked due to the LEB time and fast current slope. Dangerously high current can occur in the system if nothing is done to stop the controller. To avoid this, an additional fast comparator senses when a voltage on the current sense pin CS1 reaches $V_{CS1(stop)} = 1.5 \cdot V_{ILIM}$. If the fast comparator toggles 4 times, the controller immediately enters a protection mode. See the block diagram at Figure [2](#page-3-0) for more details.

Overvoltage Protection

An overvoltage condition, for example if the LED string is open, can be sensed at V_{out} voltage by the external resistor divider comprised of R_{ovp_top} and R_{ovp_bot} resistors (see Figure [37](#page-20-0)) which is connected to the OVP pin. If the voltage of the OVP pin exceeds the $V_{\text{OVP(off)}}$ reference voltage, the OVP fault state goes high and the switching regulator stops switching. When the voltage at OVP pin drops below the $V_{\text{OVP}(on)}$ the device starts switching again. In addition the OVP input also has under-voltage protection (UVP) to ensure the resistor divider is properly connected. If the voltage at OVP pin is below the V_{UVP} threshold the device stops.

Figure 37. Overvoltage Protection Circuit

Thermal Fold-Back

The thermal fold-back circuit reduces the current supplying to the LED string if the temperature monitored by an external NTC resistor is too high.

The current is reduced down to 0% of its nominal value. The thermal fold-back starting temperature depends on the NTC resistor value selected by the power supply designer.

The TF pin allows the direct connection of an NTC. When the TF pin voltage V_{TF} drops below $V_{TF(stat)}$, the internal reference for the constant current control V_{REF} is decreased proportionally to V_{TF} . When V_{TF} reaches $V_{TF(10\%)}$, V_{REF} is set to V_{REF10}, corresponding to 10% of the required output current. If V_{TF} drops below $V_{TF(10\%)}$ the switching regulator still reduces the VREF. If VREF drops below the 5% of its required value then the switching regulator enters the stop mode.

The thermal fold-back and OTP thresholds correspond roughly to the following resistances:

- Thermal fold-back starts when $R_{NTC} \le 11.76$ k Ω .
- Thermal fold-back sets the 10% of VREF when $R_{NTC} \leq 5.88 k\Omega$.

Figure 38. Output Current Reduction vs. TF Pin Voltage

At startup, when V_{CC} reaches $V_{CC(on)}$, the TF pin sensing is blanked for at least 300 μ s in order to allow the TF pin voltage to reach its nominal value if a filtering capacitor is connected to the TF pin. This is to avoid flickering of the LED light in case of over temperature or noise coupled to TF pin. The maximum value of OTP pin capacitor is given by the following formula (The standard start-up condition is considered and the NTC current is neglected):

$$
C_{TF \, max} = \frac{t_{TF(blank)min} \cdot l_{TF \, min}}{V_{TF(stant)max}}
$$
\n
$$
= \frac{200 \cdot 10^{-6} \cdot 80 \cdot 10^{-6}}{1.06} \, F = 15.1 \, nF
$$
\n(eq. 6)

Figure 39. Thermal Fold-Back Circuitry

Figure 40. Typical Thermal Fold-Back Characteristics when the 330 kΩ NTC and 39 kΩ Parallel Resistor **are Connected to TF Pin**

Temperature Shutdown

The NCL30167 includes a temperature shutdown protection with a trip point typically at 150°C and the typical hysteresis of 30°C. When the temperature rises above the high threshold, the switcher stops switching

instantaneously, and goes to the stop mode with low power consumption. Specific blocks are still powered from the V_{CC} supply to keep the TSD information. When the temperature falls below the low threshold, the device restarts. See the status diagrams at the Figure [29](#page-13-0).

PACKAGE DIMENSIONS

*For additional information on our Pb−Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

The product described herein (NCL30167) may be covered by one or more of U. S. patents.

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