GeneSiC SEMICONDUCTOR GA20JT12-263

Normally – OFF Silicon Carbide Junction Transistor

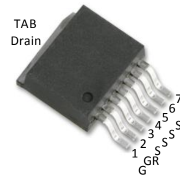
V_{DS}	=	1200 V
$R_{DS(ON)}$	=	50 mΩ
$I_{D\ (@\ 25°C)}$	=	45 A
$I_{D\ (@\ 145°C)}$	=	20 A
$h_{FE\ (@\ 25°C)}$	=	80

Features

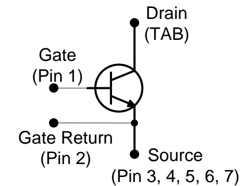
- 175 °C Maximum Operating Temperature
- Gate Oxide Free SiC Switch
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Temperature Independent Switching Performance
- Low Output Capacitance
- Positive Temperature Coefficient of $R_{DS,ON}$
- Suitable for Connecting an Anti-parallel Diode

Package

- RoHS Compliant



7L D2PAK (TO-263-7L)



Please note: The Source and Gate Return pins are not exchangeable. Their exchange might lead to malfunction.

Advantages

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20 µs Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- Minimal Input Signal Distortion
- High Amplifier Bandwidth

Applications

- Down Hole Oil Drilling, Geothermal Instrumentation
- Hybrid Electric Vehicles (HEV)
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)
- Induction Heating
- Uninterruptible Power Supply (UPS)
- Motor Drives

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Section I: Absolute Maximum Ratings

Parameter	Symbol	Conditions	Value	Unit	Notes
Drain – Source Voltage	V_{DS}	V_{GS} = 0 V	1200	V	
Continuous Drain Current	I_D	T_C = 25°C	45	A	Fig. 15
Continuous Drain Current	I_D	T_C = 145°C	20	A	Fig. 15
Continuous Gate Current	I_G		1.3	A	
Continuous Gate Return Current	I_{GR}		1.3	A	
Turn-Off Safe Operating Area	RBSOA	T_{VJ} = 175 °C, Clamped Inductive Load	$I_{D,max}$ = 20 @ $V_{DS} \le V_{DSmax}$	A	Fig. 17
Short Circuit Safe Operating Area	SCSOA	T_{VJ} = 175 °C, I_G = 1 A, V_{DS} = 800 V, Non Repetitive	>20	µs	
Reverse Gate – Source Voltage	V_{SG}		30	V	
Reverse Drain – Source Voltage	V_{SD}		25	V	
Power Dissipation	P_{tot}	T_C = 25 °C / 145 °C, t_p > 100 ms	282 / 56	W	Fig. 14
Storage Temperature	T_{stg}		-55 to 175	°C	

Section II: Static Electrical Characteristics

Parameter	Symbol	Conditions	Value Min.	Value Typical	Value Max.	Unit	Notes
A: On State							
Drain – Source On Resistance	$R_{DS(ON)}$	I_D = 20 A, T_j = 25 °C I_D = 20 A, T_j = 150 °C I_D = 20 A, T_j = 175 °C		50 93 109		mΩ	Fig. 4
Gate – Source Saturation Voltage	$V_{GS,SAT}$	I_D = 20 A, I_D/I_G = 40, T_j = 25 °C I_D = 20 A, I_D/I_G = 30, T_j = 175 °C		3.44 3.24		V	Fig. 5
DC Current Gain	h_{FE}	V_{DS} = 8 V, I_D = 20 A, T_j = 25 °C V_{DS} = 8 V, I_D = 20 A, T_j = 125 °C V_{DS} = 8 V, I_D = 20 A, T_j = 175 °C		80 55 48		–	
B: Off State							
Drain Leakage Current	I_{DSS}	V_{DS} = 1200 V, V_{GS} = 0 V, T_j = 25 °C V_{DS} = 1200 V, V_{GS} = 0 V, T_j = 150 °C V_{DS} = 1200 V, V_{GS} = 0 V, T_j = 175 °C		0.1 0.1 0.2		µA	Fig. 6
Gate Leakage Current	I_{SG}	V_{SG} = 20 V, T_j = 25 °C		20		nA	
C: Thermal							
Thermal resistance, junction - case	R_{thJC}			0.53		°C/W	Fig. 18

Section III: Dynamic Electrical Characteristics

Parameter	Symbol	Conditions	Value Min.	Value Typical	Value Max.	Unit	Notes
A: Capacitance and Gate Charge							
Input Capacitance	C_{iss}	V_{GS} = 0 V, V_{DS} = 800 V, f = 1 MHz		3091		pF	Fig. 7
Reverse Transfer/Output Capacitance	C_{rss}/C_{oss}	V_{DS} = 800 V, f = 1 MHz		53		pF	Fig. 7
Output Capacitance Stored Energy	E_{OSS}	V_{GS} = 0 V, V_{DS} = 800 V, f = 1 MHz		22		µJ	Fig. 8
Effective Output Capacitance, time related	$C_{oss,tr}$	I_D = constant, V_{GS} = 0 V, V_{DS} = 0…800 V		96		pF	
Effective Output Capacitance, energy related	$C_{oss,er}$	V_{GS} = 0 V, V_{DS} = 0…800 V		70		pF	
Gate-Source Charge	Q_{GS}	V_{GS} = -5…3 V		23		nC	
Gate-Drain Charge	Q_{GD}	V_{GS} = 0 V, V_{DS} = 0…800 V		77		nC	
Gate Charge - Total	Q_G			100		nC	
B: Switching[1]							
Internal Gate Resistance – zero bias	$R_{G(INT-ZERO)}$	f = 1 MHz, V_{AC} = 50 mV, V_{DS} = 0 V, V_{GS} = 0 V, T_j = 175 ºC		1.7		Ω	
Internal Gate Resistance – ON	$R_{G(INT-ON)}$	V_{GS} > 2.5 V, V_{DS} = 0 V, T_j = 175 ºC		0.13		Ω	
Turn On Delay Time	$t_{d(on)}$	T_j = 25 ºC, V_{DS} = 800 V, I_D = 20 A, Resistive Load Refer to Section V for additional driving information.		12		ns	
Fall Time, V_{DS}	t_f			14		ns	Fig. 9, 11
Turn Off Delay Time	$t_{d(off)}$			24		ns	
Rise Time, V_{DS}	t_r			12		ns	Fig. 10, 12
Turn On Delay Time	$t_{d(on)}$	T_j = 175 ºC, V_{DS} = 800 V, I_D = 20 A, Resistive Load		15		ns	
Fall Time, V_{DS}	t_f			13		ns	Fig. 9
Turn Off Delay Time	$t_{d(off)}$			30		ns	
Rise Time, V_{DS}	t_r			10		ns	Fig. 10
Turn-On Energy Per Pulse	E_{on}	T_j = 25 ºC, V_{DS} = 800 V, I_D = 20 A, Inductive Load Refer to Section V.		316		µJ	Fig. 9, 11
Turn-Off Energy Per Pulse	E_{off}			40		µJ	Fig. 10, 12
Total Switching Energy	E_{tot}			356		µJ	
Turn-On Energy Per Pulse	E_{on}	T_j = 175 ºC, V_{DS} = 800 V, I_D = 20 A, Inductive Load		298		µJ	Fig. 9
Turn-Off Energy Per Pulse	E_{off}			28		µJ	Fig. 10
Total Switching Energy	E_{tot}			326		µJ	

[1] – All times are relative to the Drain-Source Voltage V_{DS}

Section IV: Figures

A: Static Characteristics

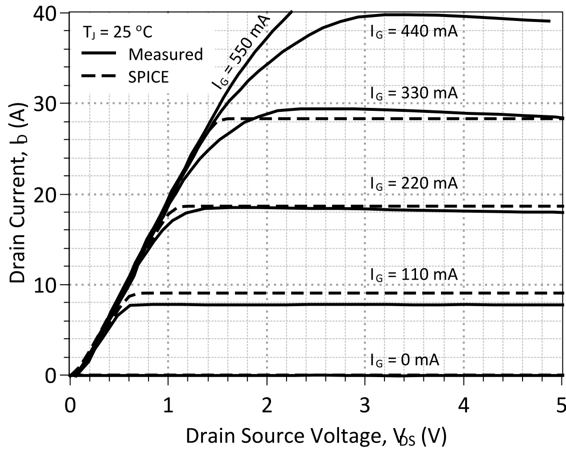


Figure 1: Typical Output Characteristics at 25 °C

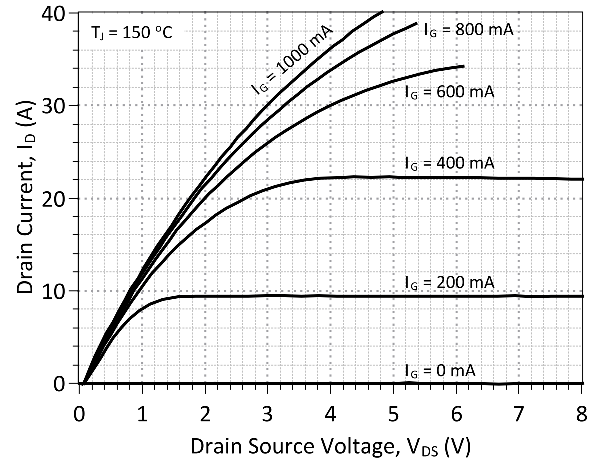


Figure 2: Typical Output Characteristics at 150 °C

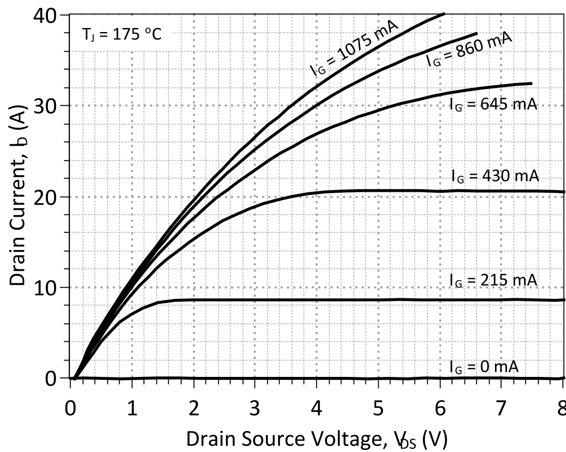


Figure 3: Typical Output Characteristics at 175 °C

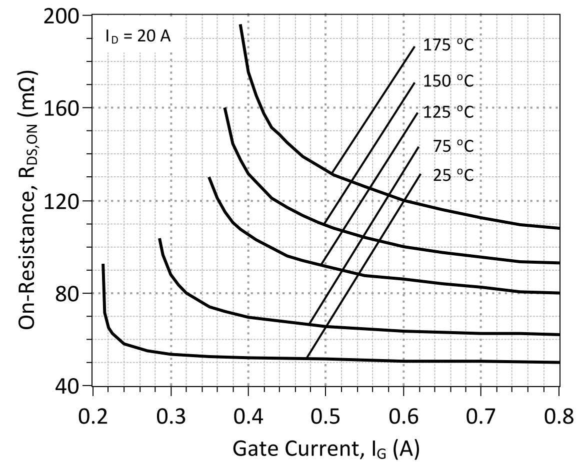


Figure 4: On-Resistance vs. Gate Current

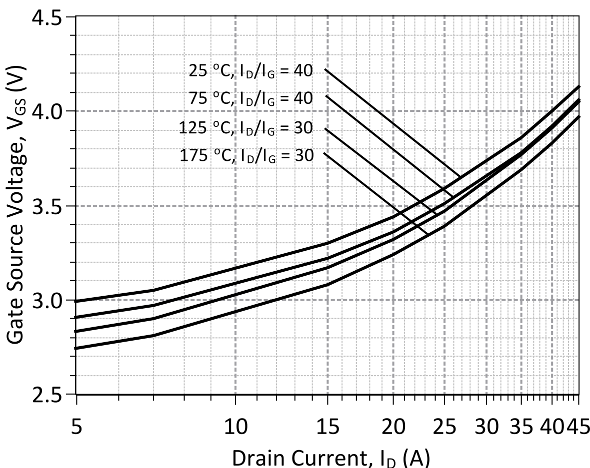


Figure 5: Typical Gate – Source Saturation Voltage

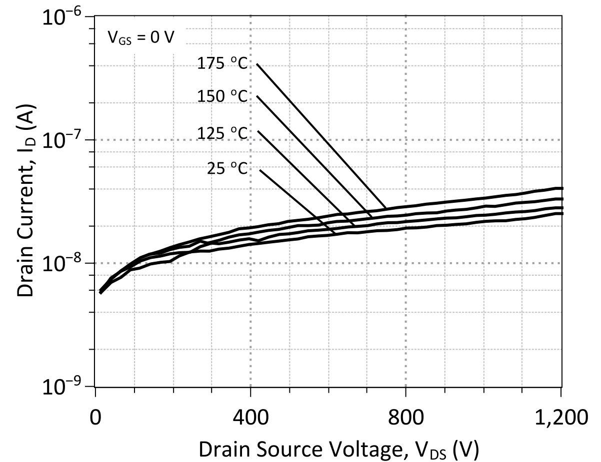


Figure 6: Typical Blocking Characteristics

B: Dynamic Characteristics

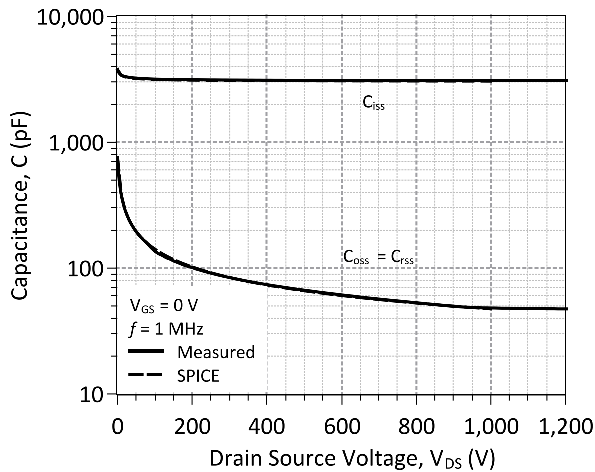


Figure 7: Input, Output, and Reverse Transfer Capacitance

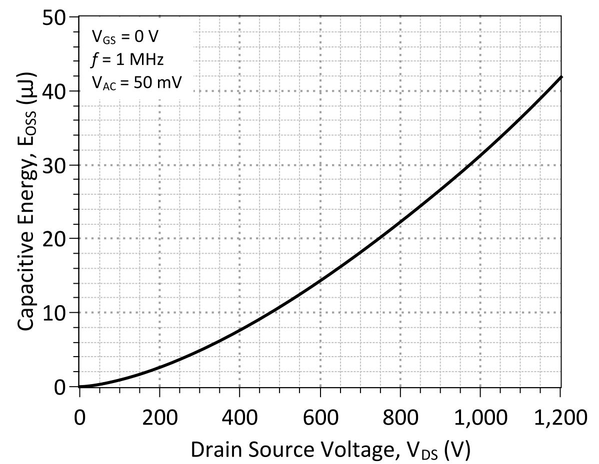


Figure 8: Energy Stored in Output Capacitance

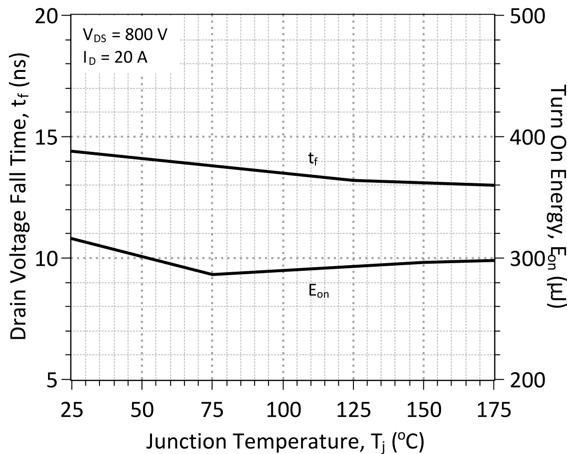


Figure 9: Typical Switching Times and Turn On Energy Losses vs. Temperature

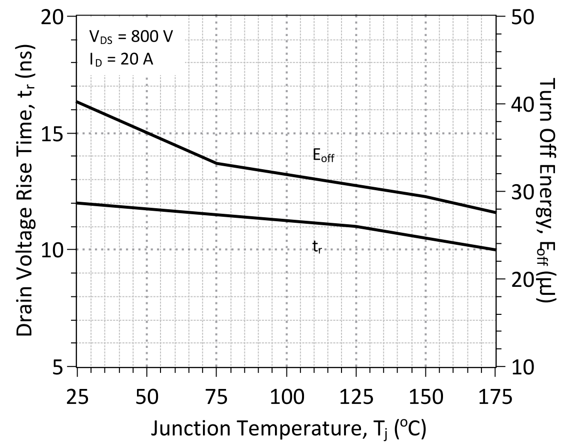


Figure 10: Typical Switching Times and Turn Off Energy Losses vs. Temperature

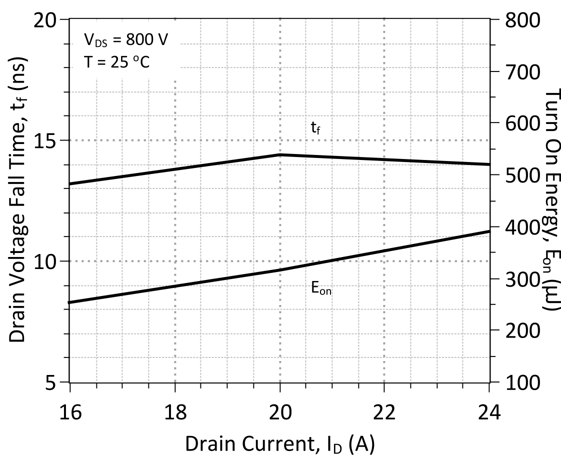


Figure 11: Typical Switching Times and Turn On Energy Losses vs. Drain Current

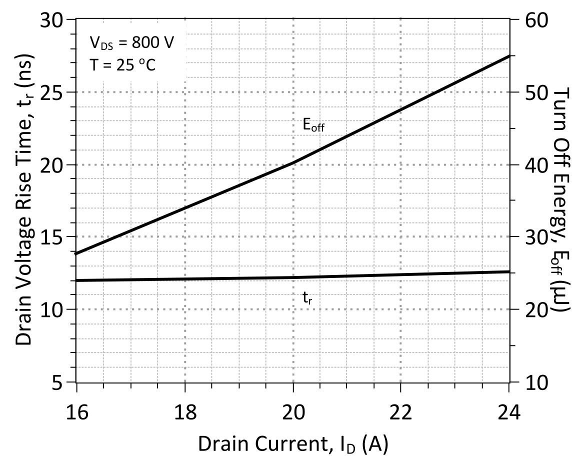


Figure 12: Typical Switching Times and Turn Off Energy Losses vs. Drain Current

C: Current and Power Derating

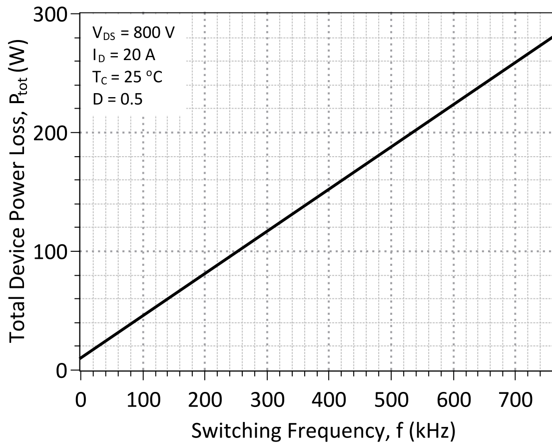


Figure 13: Typical Hard Switched Device Power Loss vs. Switching Frequency [2]

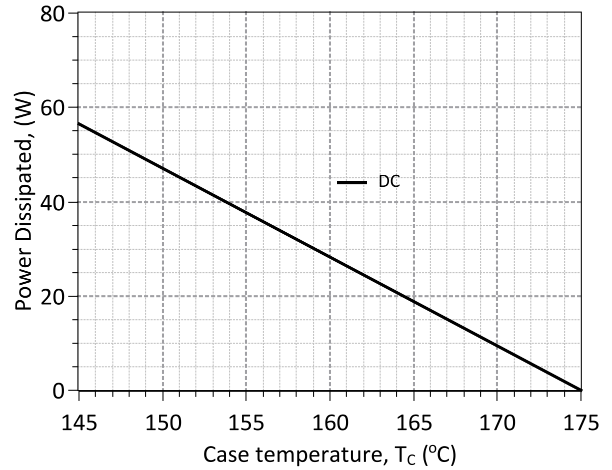


Figure 14: Power Derating Curve

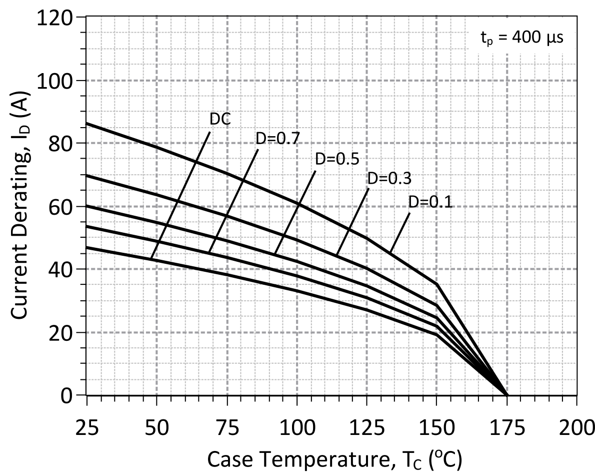


Figure 15: Drain Current Derating vs. Temperature

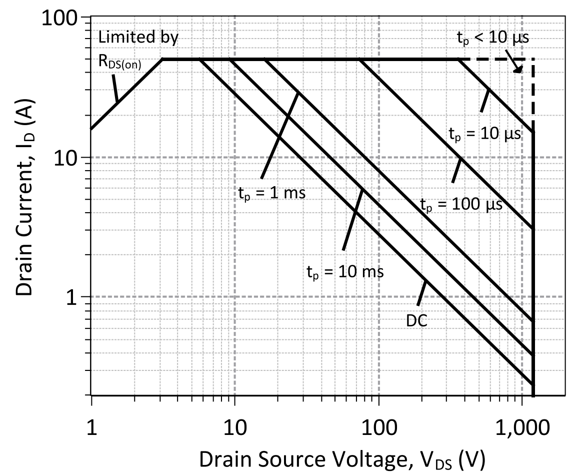


Figure 16: Forward Bias Safe Operating Area at T_c= 25 °C

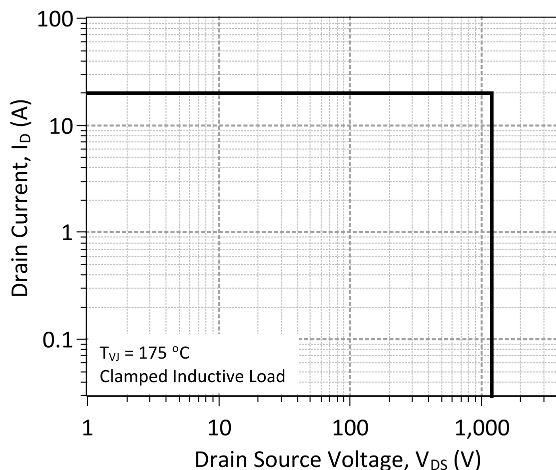


Figure 17: Turn-Off Safe Operating Area

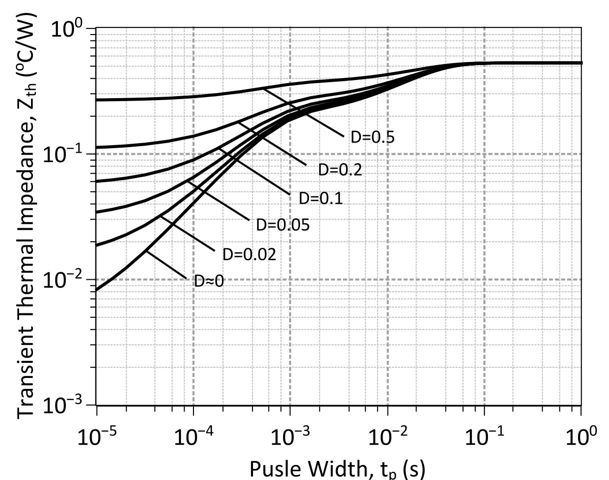


Figure 18: Transient Thermal Impedance

[2] – Representative values based on device conduction and switching loss. Actual losses will depend on gate drive conditions, device load, and circuit topology.

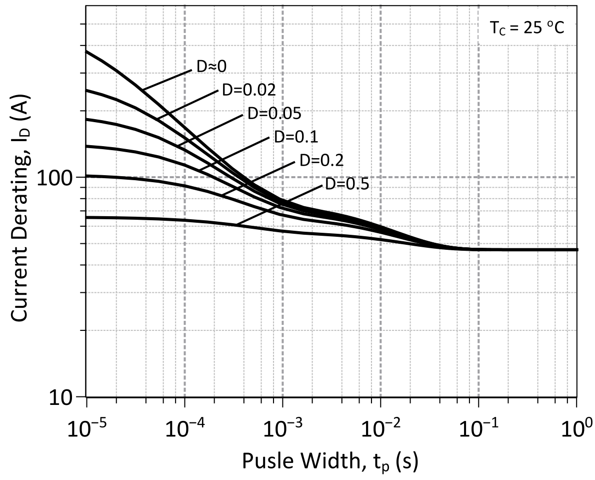


Figure 19: Drain Current Derating vs. Pulse Width

Section V: Driving the GA20JT12-263

Drive Topology	Gate Drive Power Consumption	Switching Frequency	Application Emphasis	Availability
TTL Logic	High	Low	Wide Temperature Range	Coming Soon
Constant Current	Medium	Medium	Wide Temperature Range	Coming Soon
High Speed – Boost Capacitor	Medium	High	Fast Switching	Production
High Speed – Boost Inductor	Low	High	Ultra Fast Switching	Coming Soon
Proportional	Lowest	High	Wide Drain Current Range	Coming Soon
Pulsed Power	Medium	N/A	Pulse Power	Coming Soon

A: Static TTL Logic Driving

The GA20JT12-263 may be driven using direct (5 V) TTL logic after current amplification. The (amplified) current level of the supply must meet or exceed the steady state gate current ($I_{G,steady}$) required to operate the GA20JT12-263. The power level of the supply can be estimated from the target duty cycle of the particular application. $I_{G,steady}$ is dependent on the anticipated drain current ID through the SJT and the DC current gain h_{FE}, it may be calculated from the following equation.

$$I_{G,steady} \approx \frac{I_D}{h_{FE}(T, I_D)} * 1.5$$

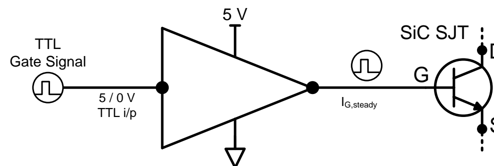


Figure 20: TTL Gate Drive Schematic

B: High Speed Driving

The SJT is a current controlled transistor which requires a positive gate current for turn-on as well as to remain in on-state. An ideal gate current waveform for ultra-fast switching of the SJT, while maintaining low gate drive losses, is shown in Figure 21 which features a positive current peak during turn-on, a negative current peak during turn-off, and continuous gate current to remain on.

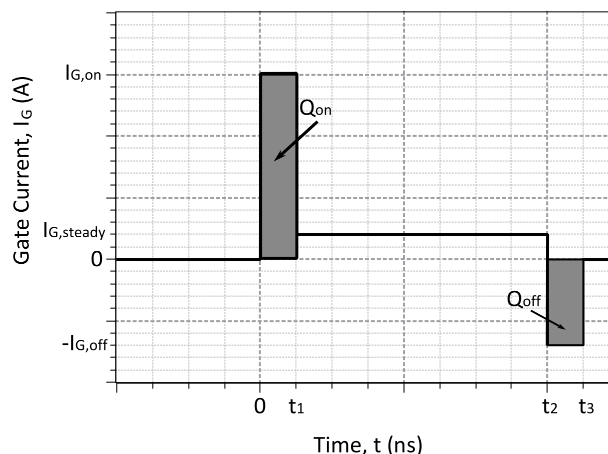


Figure 21: An idealized gate current waveform for fast switching of an SJT.

An SJT is rapidly switched from its blocking state to on-state, when the necessary gate charge, Q_G, for turn-on is supplied by a burst of high gate current, $I_{G,on}$, until the gate-source capacitance, C_{GS}, and gate-drain capacitance, C_{GD}, are fully charged.

$$Q_{on} = I_{G,on} * t_1$$

$$Q_{on} \geq Q_{gs} + Q_{gd}$$

Ideally, $I_{G,pon}$ should terminate when the drain voltage falls to its on-state value in order to avoid unnecessary drive losses during the steady on-state. In practice, the rise time of the $I_{G,on}$ pulse is affected by the parasitic inductances, L_{par} in the device package and drive circuit. A voltage developed across the parasitic inductance in the source path, L_s, can de-bias the gate-source junction, when high drain currents begin to flow through the device. The voltage applied to the gate pin should be maintained high enough, above the $V_{GS,sat}$ (see Figure 5) level to counter these effects.

A high negative peak current, $-I_{G,off}$ is recommended at the start of the turn-off transition, in order to rapidly sweep out the injected carriers from the gate, and achieve rapid turn-off. While satisfactory turn off can be achieved with V_{GS} = 0 V, a negative gate voltage V_{GS} may be used in order to speed up the turn-off transition.

Two high-speed drive topologies for the SiC SJTs are presented below.

B:1: High Speed, Low Loss Drive with Boost Capacitor, GA03IDDJT30-FR4

The GA20JT12-263 may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide fast switching current peaks at turn-on and turn-off and a continuous gate current while in on-state. A 3 kV isolated evaluation gate drive board (GA03IDDJT30-FR4) utilizing this topology is commercially available for high and low-side driving, its datasheet provides additional details about this drive topology.

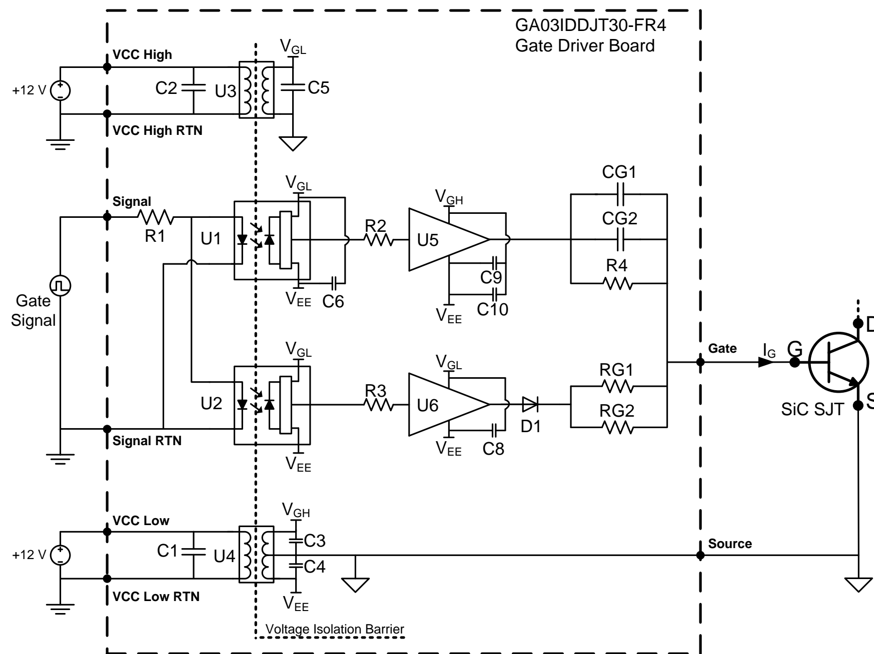


Figure 22: Topology of the GA03IDDJT30-FR4 Two Voltage Source gate driver.

The GA03IDDJT30-FR4 evaluation board comes equipped with two on board gate drive resistors (RG1, RG2) pre-installed for an effective gate resistance[3] of R_G = 3.75 Ω. It may be necessary for the user to reduce RG1 and RG2 under high drain current conditions for safe operation of the GA20JT12-263. The steady state current supplied to the gate pin of the GA20JT12-263 with on-board R_G = 3.75 Ω, is shown in Figure 23. The maximum allowable safe value of R_G for the user's required drain current can be read from Figure 24.

For the GA20JT12-263, R_G must be reduced for $I_D \geq$ ~13 A for safe operation with the GA03IDDJT30-FR4.

For operation at $I_D \geq$ ~13 A, R_G may be calculated from the following equation, which contains the DC current gain h_{FE} and the gate-source saturation voltage $V_{GS,sat}$ (Figure 5).

$$R_{G,max} = \frac{\left(4.7V - V_{GS,sat}\right) * h_{FE}(T, I_D)}{I_D * 1.5} - 0.6\Omega$$

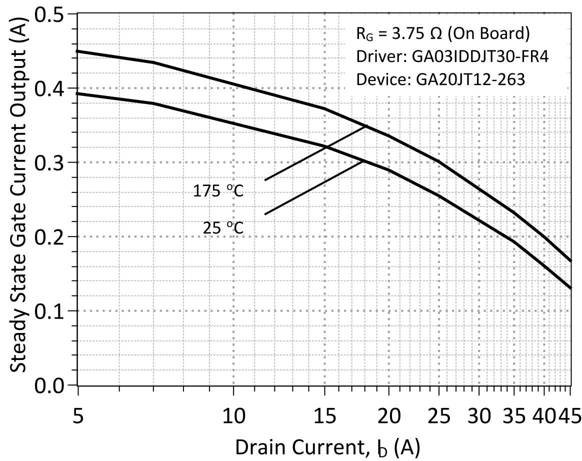


Figure 23: Typical steady state gate current supplied by the GA03IDDJT30-FR4 board for the GA20JT12-263 with the on board resistance of 3.75 Ω

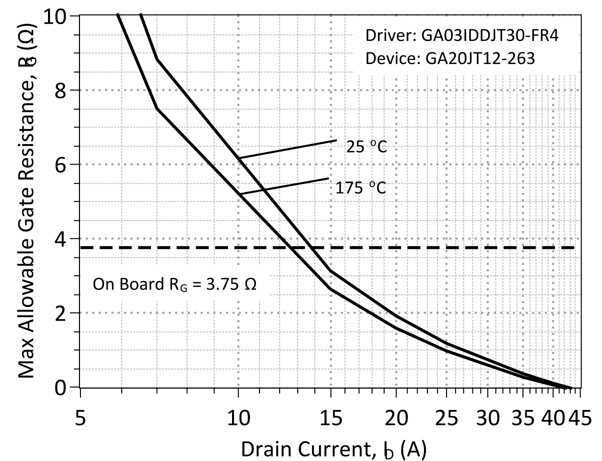


Figure 24: Maximum gate resistance for safe operation of the GA20JT12-263 at different drain currents using the GA03IDDJT30-FR4 board.

B:2: High Speed, Low Loss Drive with Boost Inductor

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the GA20JT12-263 at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses $I_{G,on}$ and $I_{G,off}$. During operation, inductor L is charged to a specified $I_{G,on}$ current value then made to discharge I_L into the SJT gate pin using logic control of S_1, S_2, S_3, and S_4, as shown in Figure 25. After turn on, while the device remains on the necessary steady state gate current $I_{G,steady}$ is supplied from source V_{CC} through R_G. Please refer to the article "A current-source concept for fast and efficient driving of silicon carbide transistors" by Dr. Jacek Rąbkowski for additional information on this driving topology.[4]

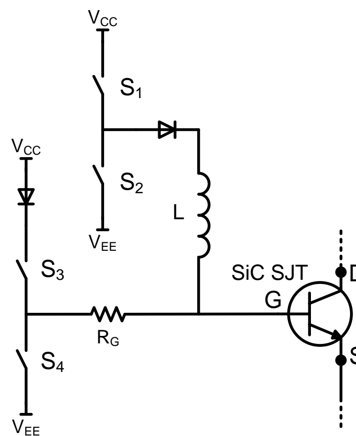


Figure 25: Simplified Inductive Pulsed Drive Topology

[3] – $R_G = (1/RG1 + 1/RG2)^{-1}$. Driver is pre-installed with RG1 = RG2 = 7.5 Ω

[4] – Archives of Electrical Engineering. Volume 62, Issue 2, Pages 333–343, ISSN (Print) 0004-0746, DOI: 10.2478/aee-2013-0026, June 2013

C: Proportional Gate Current Driving

For applications in which the GA20JT12-263 will operate over a wide range of drain current conditions, it may be beneficial to drive the device using a proportional gate drive topology to optimize gate drive power consumption. A proportional gate driver relies on instantaneous drain current I_D feedback to vary the steady state gate current $I_{G,steady}$ supplied to the GA20JT12-263

C:1: Voltage Controlled Proportional Driver

The voltage controlled proportional driver relies on a gate drive IC to detect the GA20JT12-263 drain-source voltage V_{DS} during on-state to sense I_D. The gate drive IC will then increase or decrease $I_{G,steady}$ in response to I_D. This allows $I_{G,steady}$, and thus the gate drive power consumption, to be reduced while I_D is relatively low or for $I_{G,steady}$ to increase when is I_D higher. A high voltage diode connected between the drain and sense protects the IC from high-voltage when the driver and GA20JT12-263 are in off-state. A simplified version of this topology is shown in Figure 27, additional information will be available in the future at http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/

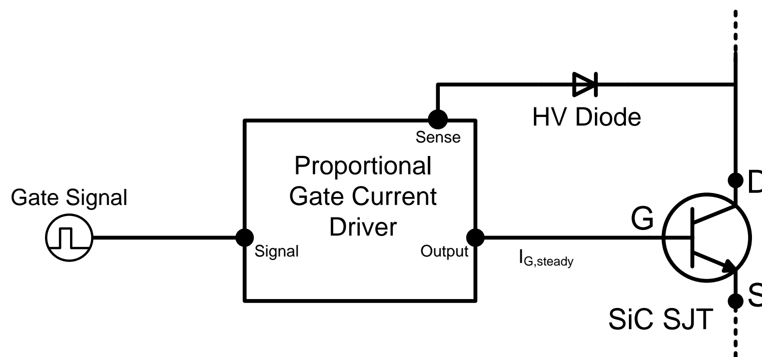


Figure 26: Simplified Voltage Controlled Proportional Driver

C:2: Current Controlled Proportional Driver

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback I_D of the GA20JT12-263 during on-state to supply $I_{G,steady}$ into the device gate. $I_{G,steady}$ will then increase or decrease in response to I_D at a fixed forced current gain which is set be the turns ratio of the transformer, $h_{force} = I_D / I_G = N_2 / N_1$. GA20JT12-263 is initially tuned-on using a gate current pulse supplied into an RC drive circuit to allow I_D current to begin flowing. This topology allows $I_{G,steady}$, and thus the gate drive power consumption, to be reduced while I_D is relatively low or for $I_{G,steady}$ to increase when is I_D higher. A simplified version of this topology is shown in Figure 27, additional information will be available in the future at http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/.

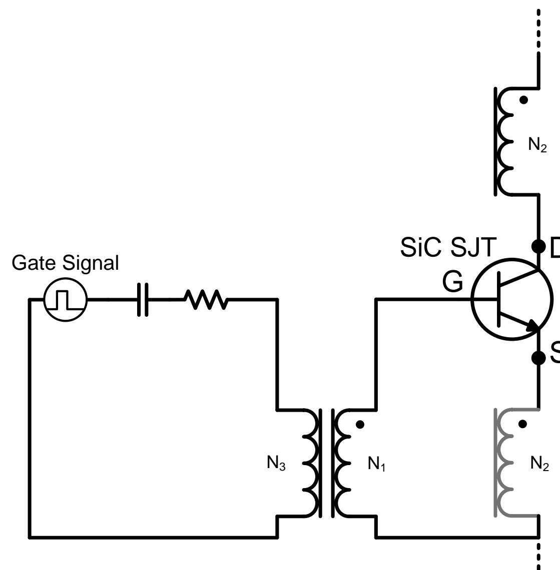
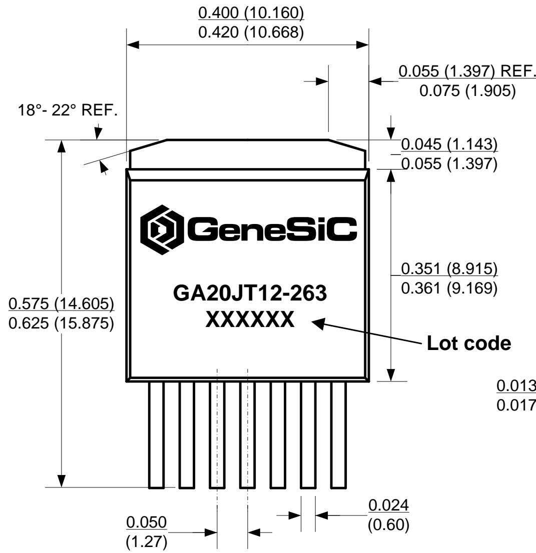
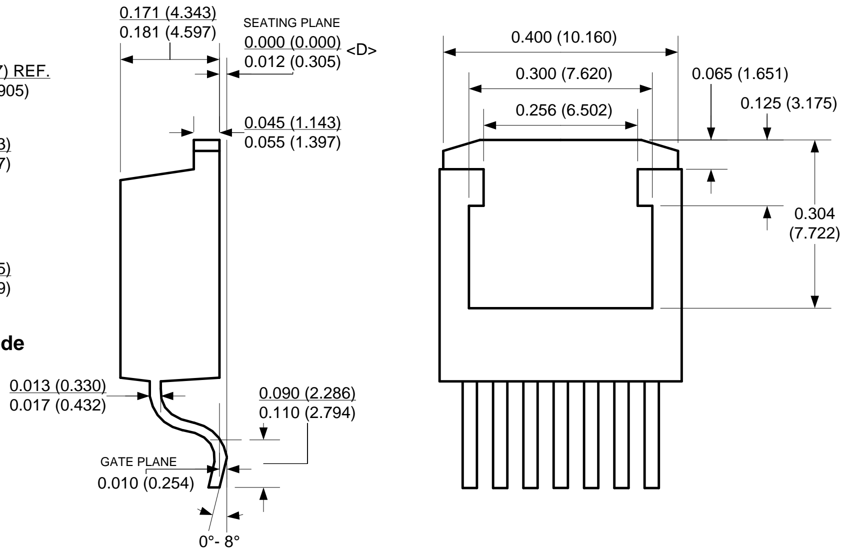


Figure 27: Simplified Current Controlled Proportional Driver

Section VI: Package Dimensions

TO-263-7L **PACKAGE OUTLINE**





NOTE
1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.
2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS

Revision History			
Date	Revision	Comments	Supersedes
2015/06/05	0	Initial release	

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Section VII: SPICE Model Parameters

This is a secure document. Please copy this code from the SPICE model PDF file on our website (http://www.genesicsemi.com/images/products_sic/sjt/GA20JT12-263_SPICE.pdf) into LTSPICE (version 4) software for simulation of the GA20JT12-263.

```
*     MODEL OF GeneSiC Semiconductor Inc.
*
*     $Revision:   1.0           $
*     $Date:   05-JUN-2015       $
*
*     GeneSiC Semiconductor Inc.
*     43670 Trade Center Place Ste. 155
*     Dulles, VA 20166
*
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*
* These models are provided "AS IS, WHERE IS, AND WITH NO WARRANTY
* OF ANY KIND EITHER EXPRESSED OR IMPLIED, INCLUDING BUT NOT LIMITED
* TO ANY IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A
* PARTICULAR PURPOSE."
* Models accurate up to 2 times rated drain current.
*
.model GA20JT12 NPN
+ IS       9.833E-48
+ ISE      1.073E-26
+ EG       3.23
+ BF       80
+ BR       0.55
+ IKF      5000
+ NF       1
+ NE       2
+ RB       3.09
+ IRB      0.006
+ RBM      0.101
+ RE       0.005
+ RC       0.040
+ CJC      752.4E-12
+ VJC      3.17
+ MJC      0.480
+ CJE      3.014E-09
+ VJE      3.568
+ MJE      0.538
+ XTI      3
+ XTB      -1.5
+ TRC1     8.500E-3
+ VCEO     1200
+ ICRATING 20
+ MFG      GeneSiC_Semiconductor
*
* End of GA20JT12 SPICE Model
```

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